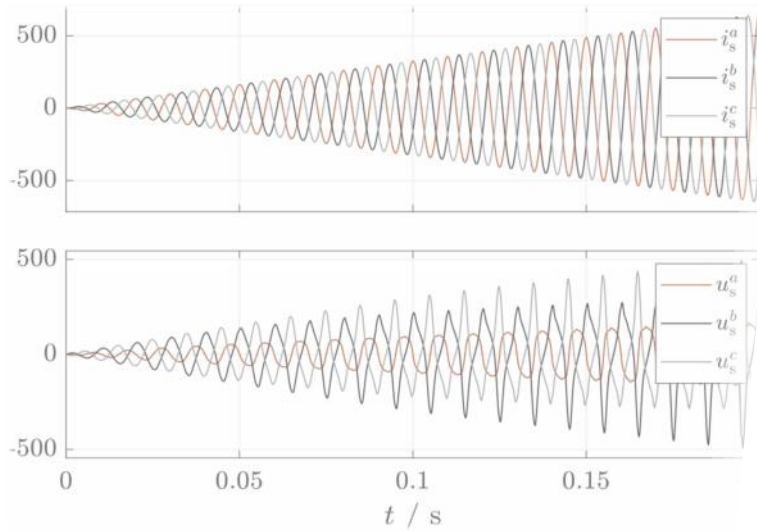


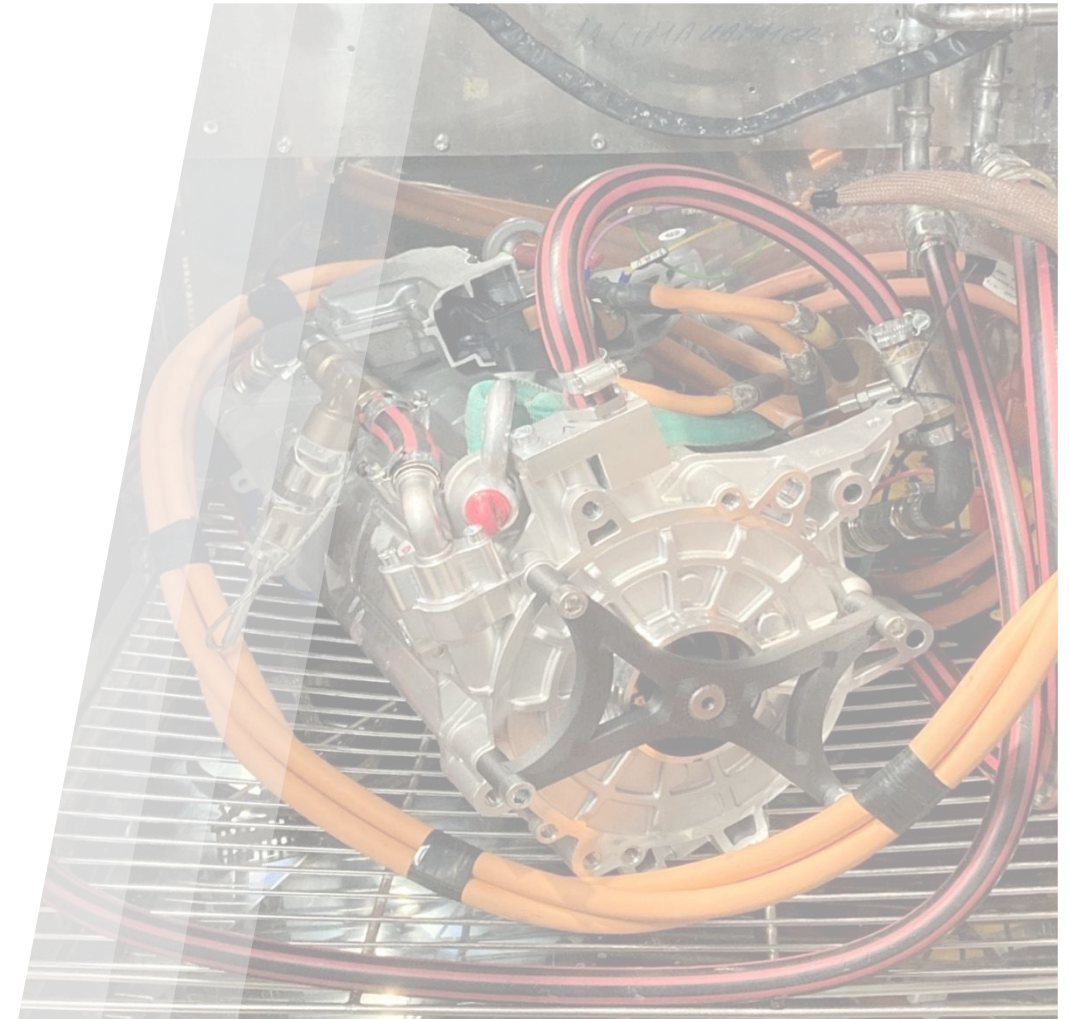


E-Motor parameter identification: Possibilities from theory to vehicle

Johannes KÖLBL
Bernd PFEIFER
Christian SCHMIDT

E-Motor parameter identification: Possibilities from theory to vehicle

1. **Personal introduction & motivation**
2. **Parameter identification**
 - a. static on dyno test bench
 - b. dynamic with ERA
3. **Evaluations**
 - a. dyno vs. ERA
 - b. on vehicle level
4. **Series identification with ERA**
5. **Summary & outlook**



Personal introduction & motivation



Personal introduction



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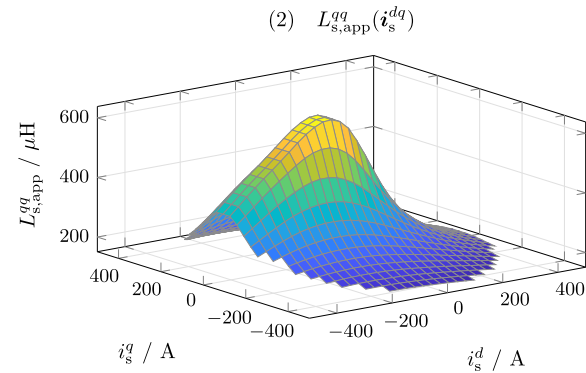
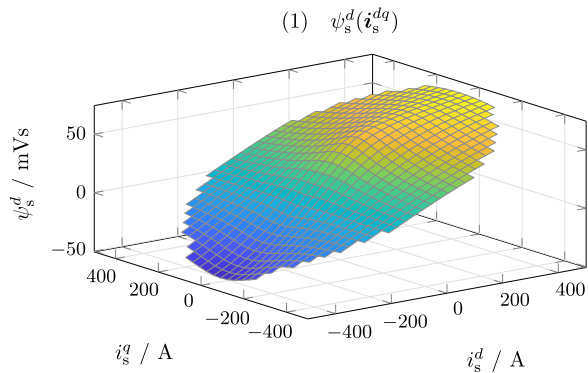
AVL inverter TS™ @ AVL SET
Wangen im Allgäu

Cooperation project:
CE³ - Comparison of electric cars, electric drive dyno, and electric motor emulator

Motivation

- Torque/speed control of electrical drives requires a parametrized machine model
 - Parameters vary per machine and per operating point
 - More detailed and individual parameters
- More robust, dynamic and efficient control

Efficient electrical drive operation requires accurate machine parameters



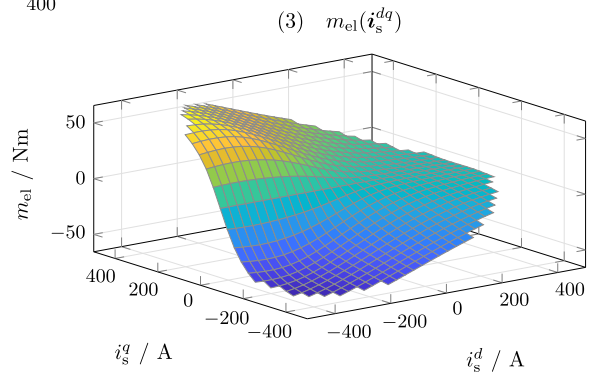
Parameter name	Parameter
Stator resistance	$R_s^{abc}(\vartheta_s)$
Stator flux linkage maps (1)	$\psi_s^{dq}(i_s^{dq}, \vartheta_s)$
↪ Permanent magnet flux linkage	$\psi_{pm}^{dq}(i_s^q, \vartheta_s)$
↪ Apparent inductance maps (2)	$L_{s,app}^{dq}(i_s^{dq}, \vartheta_s)$
↪ Differential inductance maps	$L_{s,diff}^{dq}(i_s^{dq}, \vartheta_s)$
↪ Torque maps (3)	$m_{el}(i_s^{dq}, \vartheta_s)$

with stator currents i_s^{dq} and stator temperature ϑ_s

$$\psi_s^{dq} = \psi_{pm}^{dq} + L_{s,app}^{dq} i_s^{dq}$$

$$m_{el} = \frac{3n_p}{2} (i_s^{dq})^T J \psi_s^{dq}$$

Fundamental and derived electromagnetic machine parameters as functions of stator currents and stator temperature.



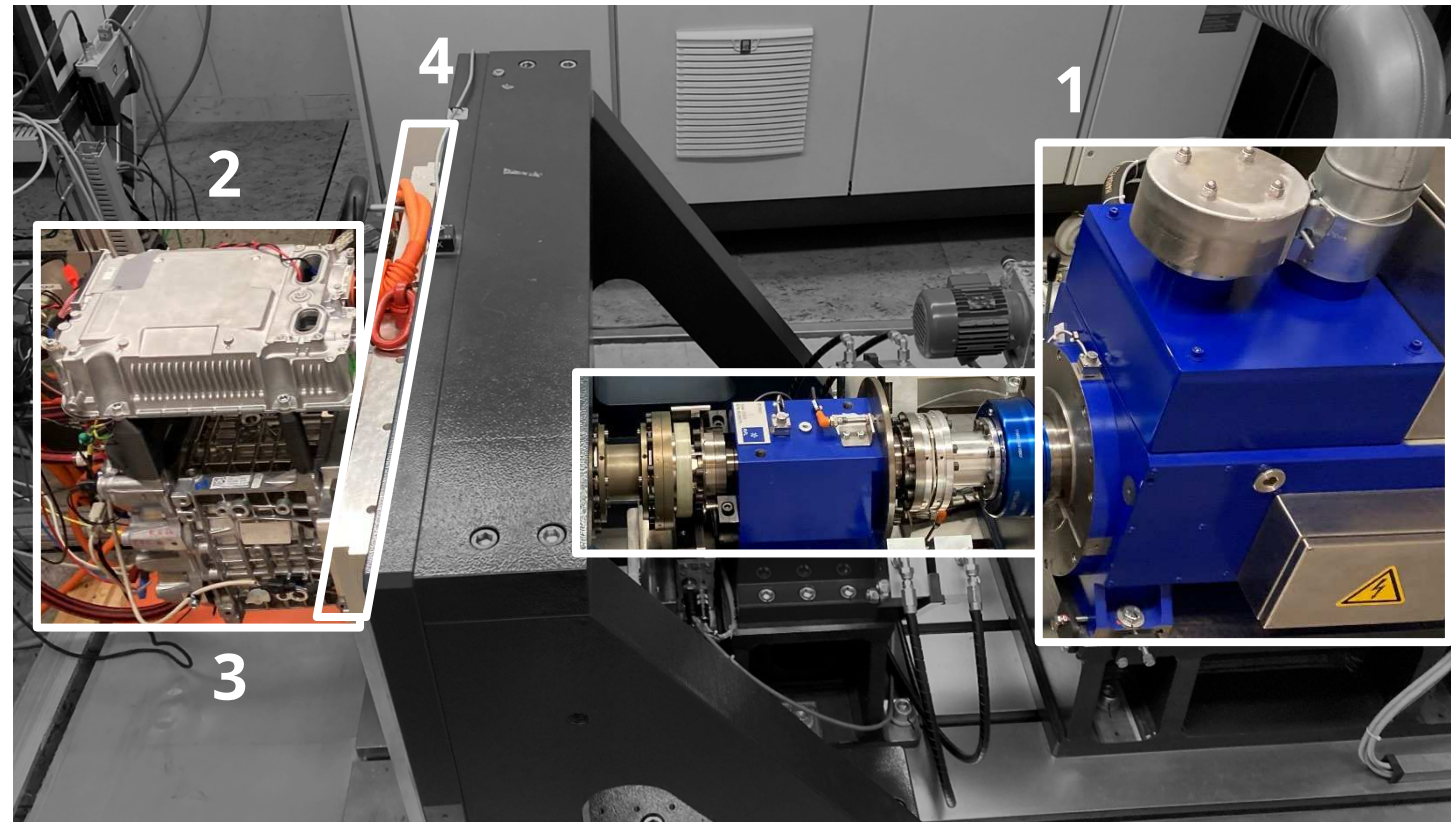
Static parameter identification on dyno test bench

2.a

Static parameter identification on dyno test bench

Test bench

1. Single-ended dyno test bench with external measurement system
2. High performance inverter
→ individual **I_d / I_q controlling** necessary
3. Prepared electric machine **without** reducer
4. Test bench adaptation
→ **specific** adapter plate, shaft and coupling
5. Dyno booking, test execution and personnel



Time and cost are primarily driven by manufacturing adaptation, test execution and personnel

Static parameter identification on dyno test bench

Challenge

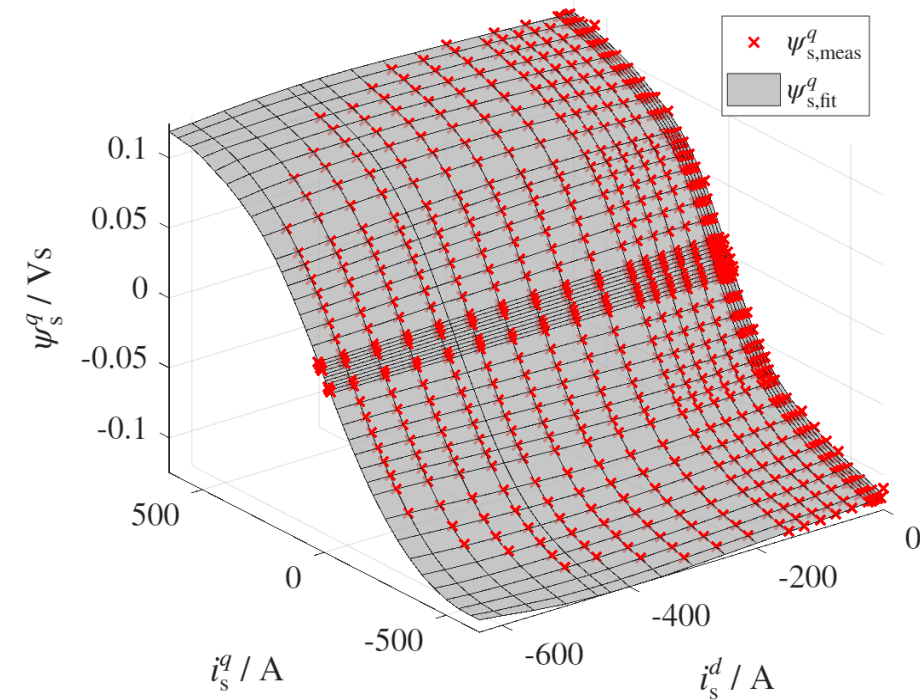
Stable steady-state working points

→ Identical conditions for
speed
voltage
rotor temperature

over complete Id-Iq-current map

Procedure

- Four-wire resistance measurement of stator
- Automatic test routine with
 - **BackEMF** measurement for PM flux linkage
 - **Id-Iq-current map** for stator flux linkage
- Parameter postprocessing offline with Schaeffler tool



Accurate identification of d/q-axis stator flux-linkage maps under identical conditions

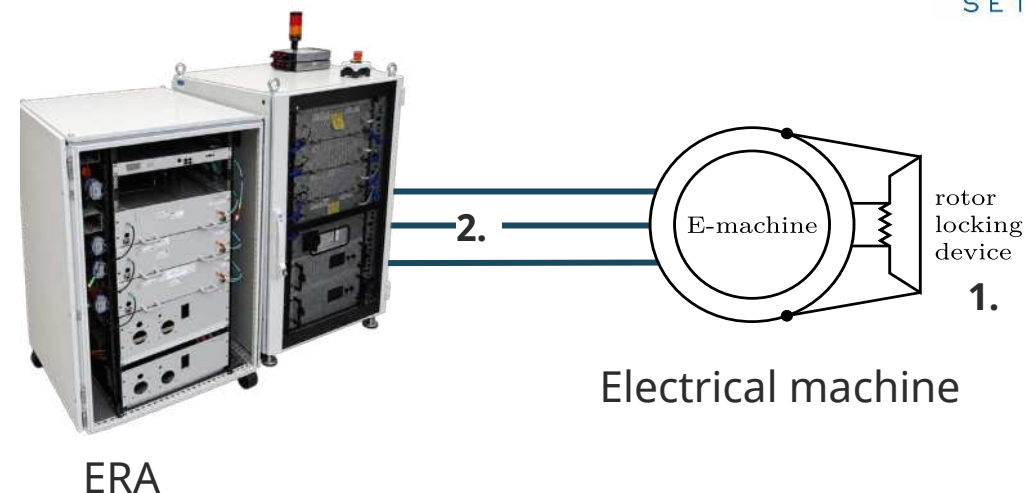
Dynamic parameter identification with ERA

2.b

Basic idea – Electric machine Rapid Analyzer (ERA)

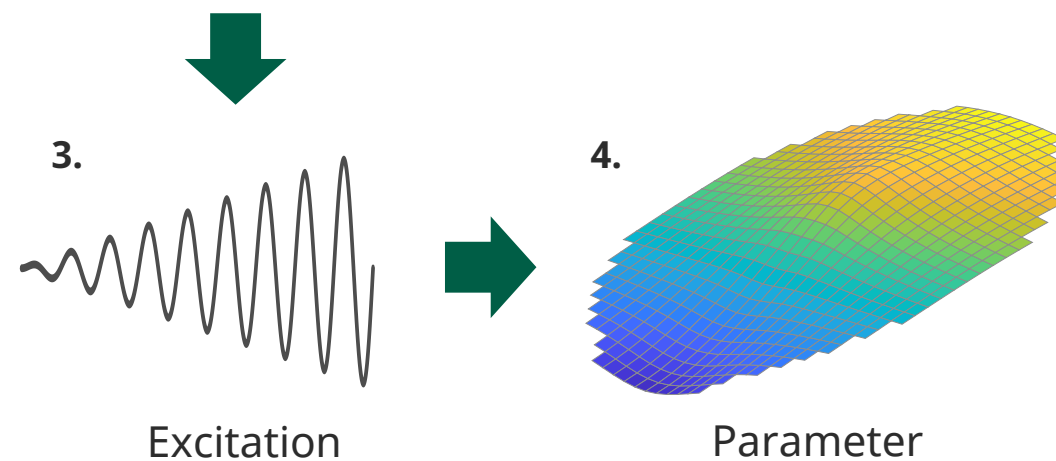
Test bench (AVL Inverter TS™)

- Robust current injection into unknown traction machines, enabled by high-performance multi-level topology
- Precise built-in voltage and current measurement, sampling rate up to 3.125 MHz (320 ns)
- The ERA is a hardware-reduced version of the AVL inverter TS™.



Procedure

1. Block rotor or connect rotor position sensor (RPS)
2. Connect the three-phase power cables
3. Inject highly dynamic current excitation
4. Identify machine parameters from the measured currents and voltages



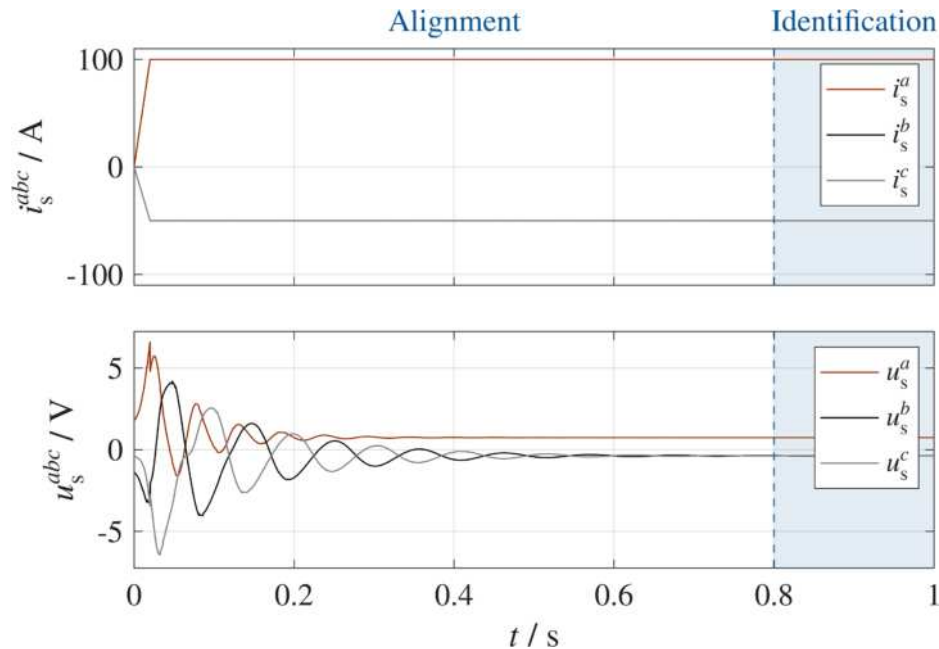
ERA used for machine parameter identification

TS: test system; RPS: rotor position sensor

Identification scenario for resistance and permanent magnet (PM) flux linkage

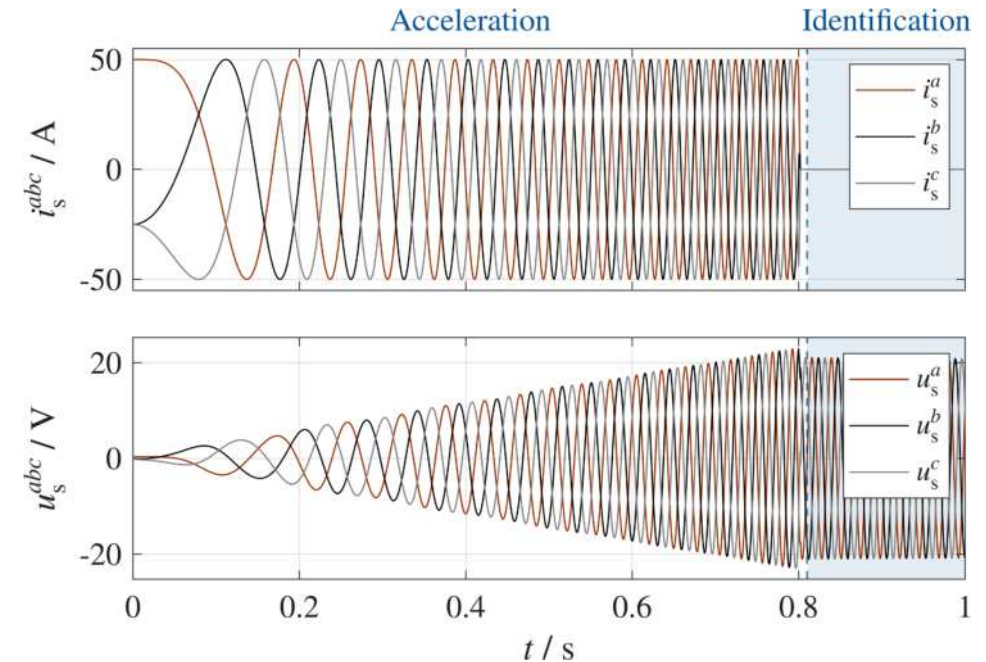
Resistance:

- **Alignment:** DC injection pulls the rotor d-axis onto the a-axis
- **Identification:** After alignment, resistance is identified from measured voltages and currents



PM flux linkage:

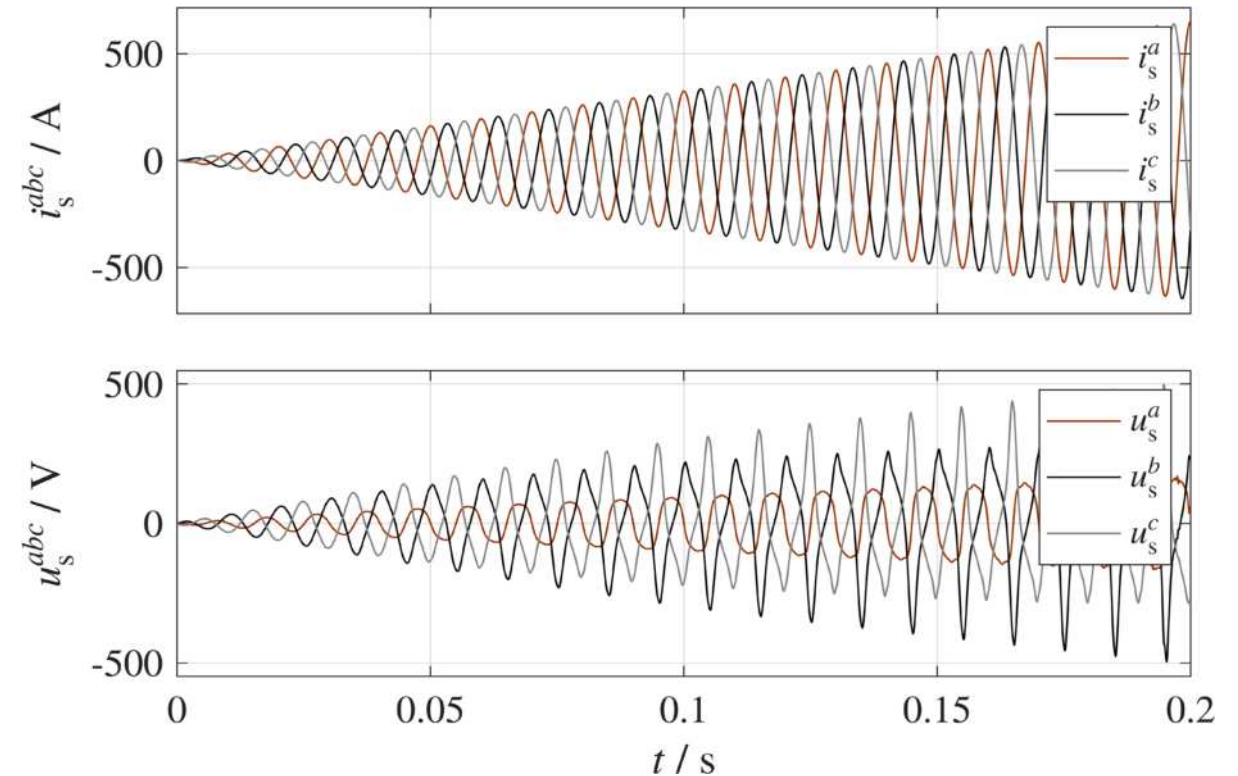
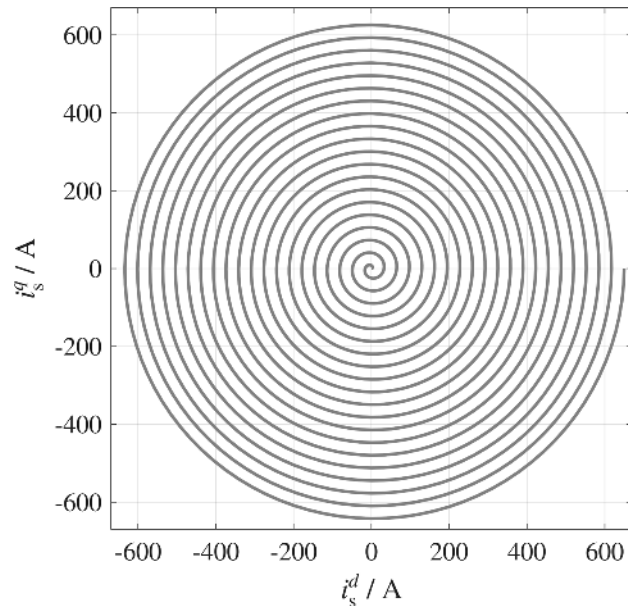
- **Acceleration:** AC injection accelerates the rotor from zero to reference speed
- **Identification:** After acceleration, switches are opened and PM flux linkage is identified from the back-EMF voltage



Identification of resistance and PM flux done in advance

Identification scenario for inductances

- **Objective:** cover all operating points of interest in minimum time, while accounting for
- Hardware limits: maximum voltage, current, speed
- Physical effects: e.g. iron losses, excited by the current dynamics of the injection scenario



Machine parameters are identified through dynamic current injection

Postprocessing – Measurements to parameter

Signal preparation

- Signal filtering and compensation for sensor measurement errors
- Signal filtering to reduce measurement noise
- (Rotor position evaluation)

Identification

- Identification of resistance
- Identification of permanent magnet flux linkage [10]
- Identification of stator flux linkage maps based on differential flux linkage equation

Parameter fitting

- Identification and compensation of flux linkage tilting due to physical iron effects
- Physical informed fitting of flux linkage maps
- Transfer of identified flux linkage maps to user environments
- (Compensation of cable)

Comparison dyno vs. ERA identification

3.a

Comparison dyno vs. ERA

	Component	Dyno system	ERA system
General	Test bench	Single-ended dyno (1ED)	ERA
	AC inverter	1x	integrated
	Test bench adaptation	Adapter-plate Shaft Coupling	Rotor locking device
	Testrun	Automated	Manual or automated
Measurement	Power Analyzer	External	External / integrated
	Current sensor	External	External / integrated
	Voltage sensor	External	External / integrated
	Temperature	(1x)	-
	Torque	(1x)	-
	Rotor position sensor (RPS)	1x	(1x)

Reduced effort with ERA-based parameter identification

ERA: E-machine Rapid Analyzer; RPS: rotor position sensor

Comparison dyno vs. ERA

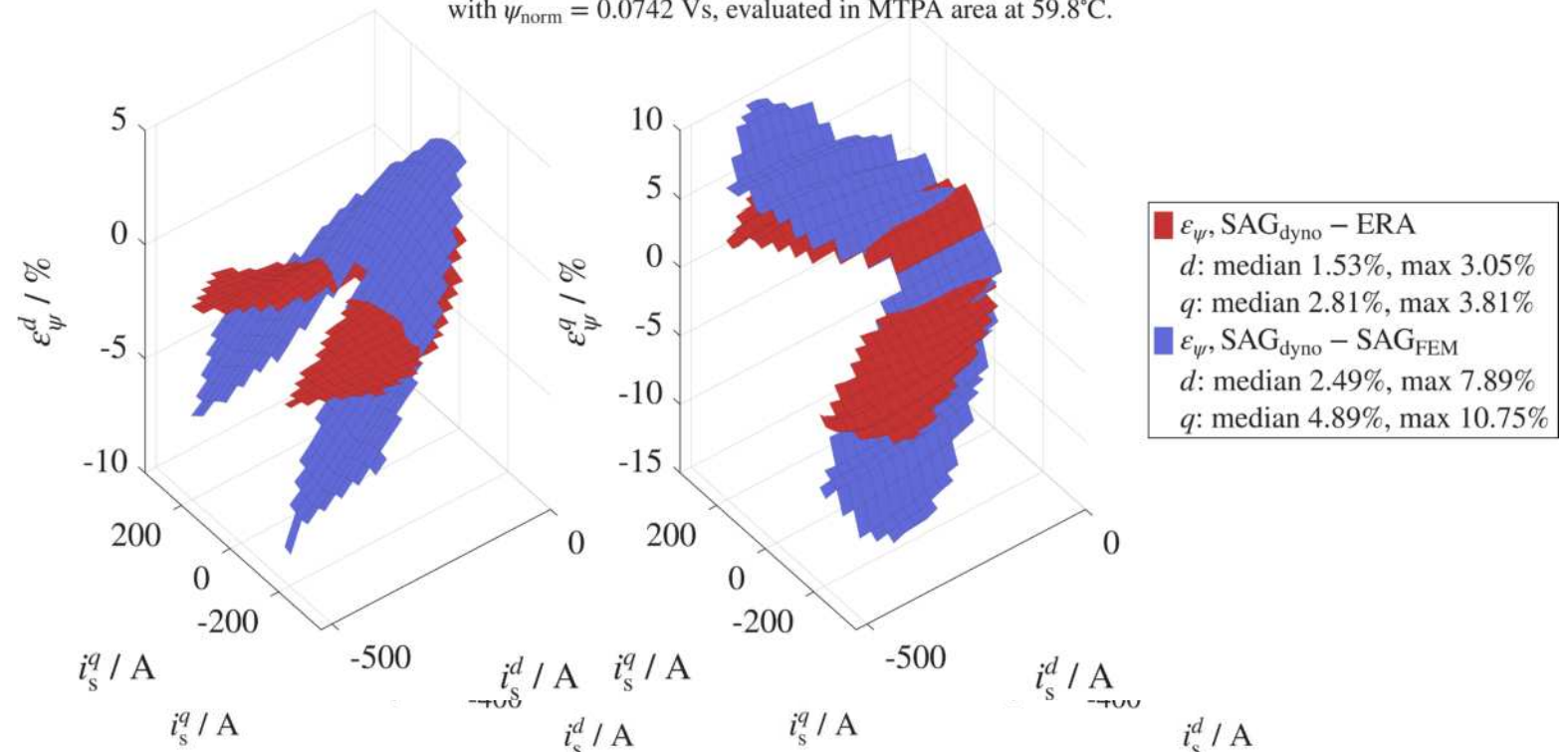
Parameter

Torque accuracy

System efficiency

- Stator flux linkage maps
- MTPA area
- Calculated LUTs from dyno
 - vs. ERA
 - vs. FEM

Flux linkage maps comparison in MTPA area of IPM EMR3 at 59.8°C.
 Relative error of flux linkage maps $\varepsilon_{\psi}^{dq} = (\psi_{s,SAG_{dyno}}^{dq} - \psi_{s,x}^{dq}) / \psi_{norm} \cdot 100$ of IPM EMR3,
 with $\psi_{norm} = 0.0742$ Vs, evaluated in MTPA area at 59.8°C.



Comparison dyno vs. ERA

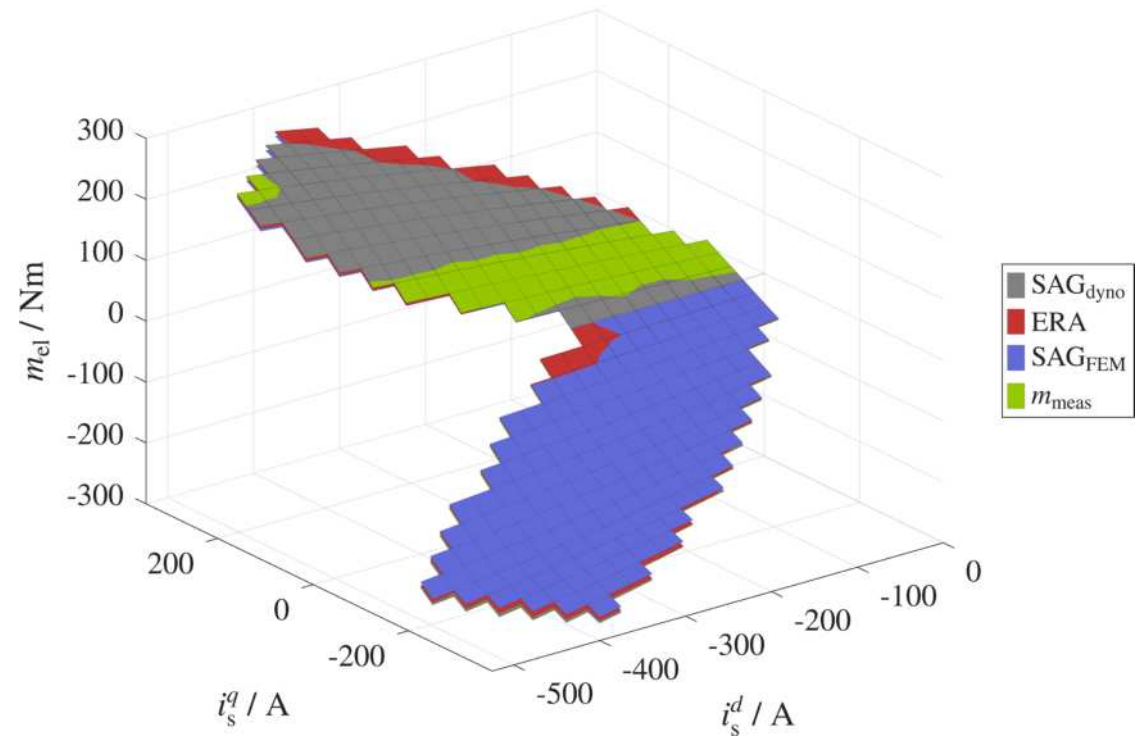
Parameter

Torque accuracy

System efficiency

- Dyno torque (i_d -/ i_q -map)
- MTPA area
- Measured torque from dyno vs. inverter calculated with
 - dyno identification
 - ERA identification
 - FEM simulation

Torque maps comparison in MTPA area of IPM EMR3 at 59.8°C.



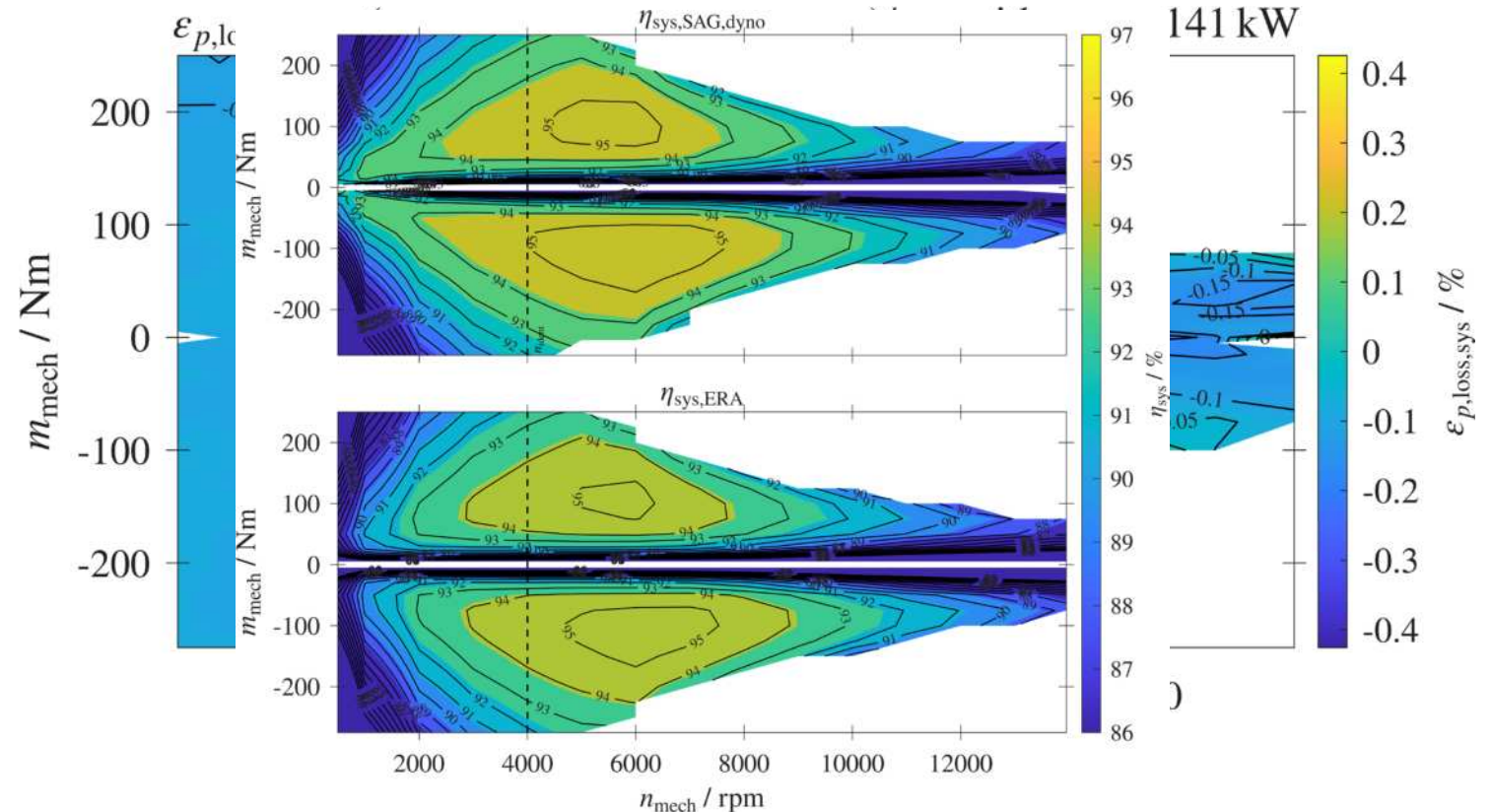
Comparison dyno vs. ERA

Parameter

Torque accuracy

System efficiency

- Torque-speed-map
- System efficiency
 - mot: $P_{\text{mech}} / P_{\text{DC}}$
 - gen: $P_{\text{DC}} / P_{\text{mech}}$
- Efficiency with
 - dyno identification
 - ERA identification

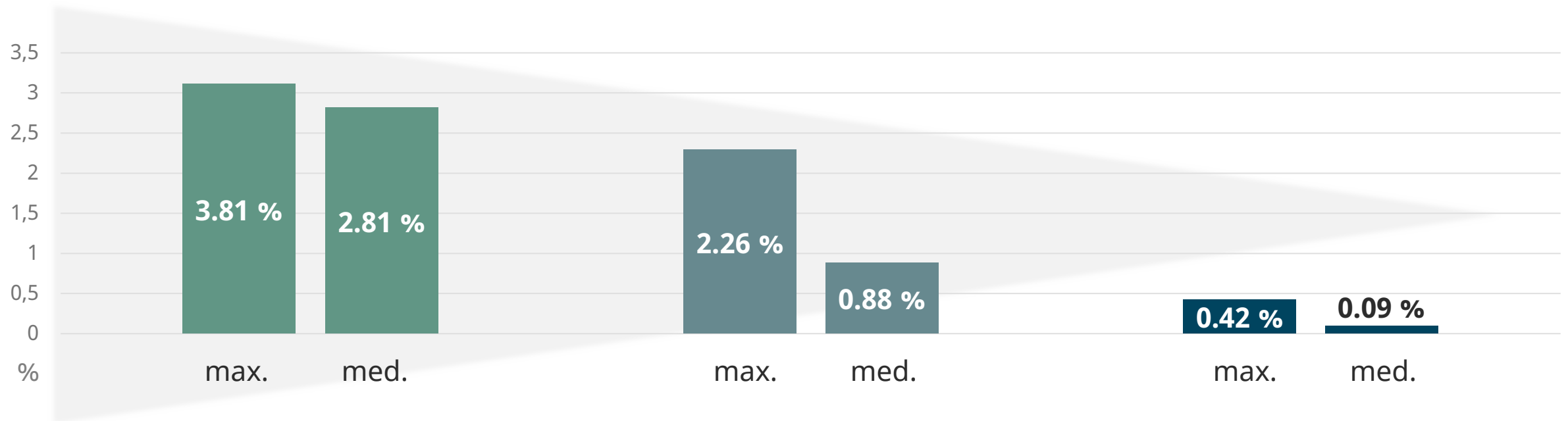


Comparison dyno vs. ERA

Parameter

Torque accuracy

System efficiency



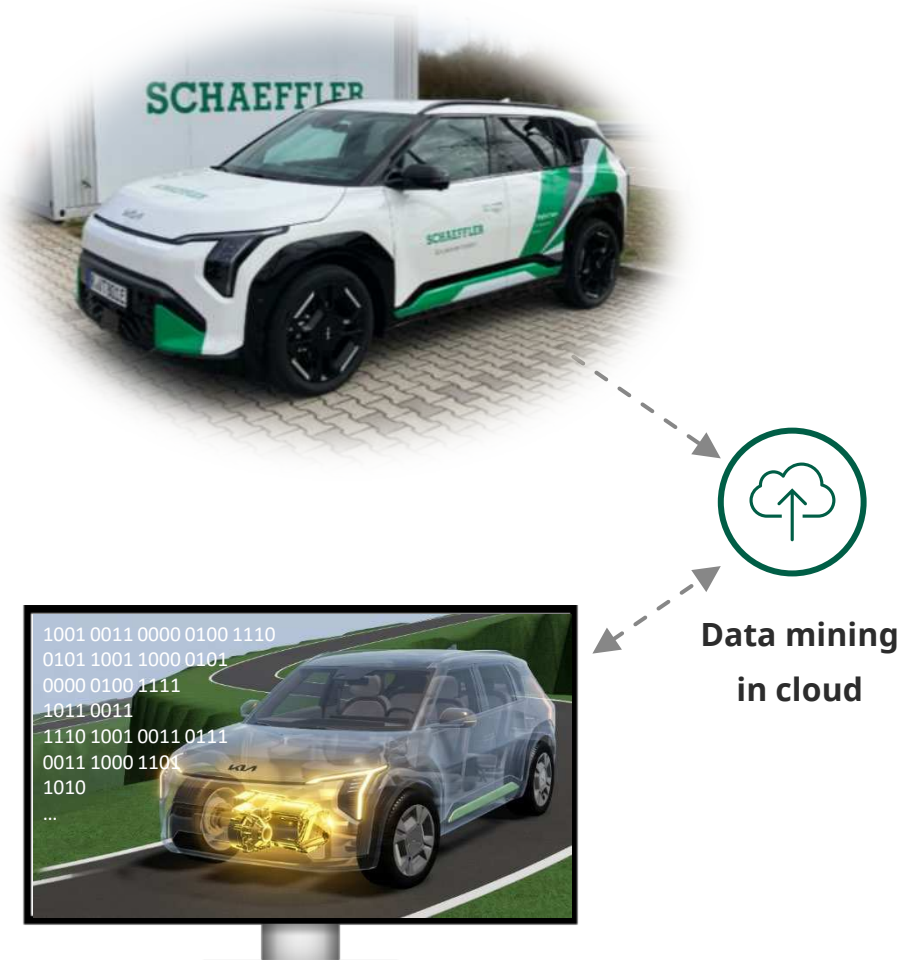
ERA-based identification delivers results comparable to dyno-based identification

ERA: E-machine Rapid Analyzer; max: maximum; med: median

Evaluations on vehicle level

3.b

Evaluations on vehicle level with 400 V development vehicle – SC.EV32



Virtual development using “Digital Twin”

EMR4: E-drivetrain 4th generation; ERA: E-machine Rapid Analyzer; LTE: long term evolution

September, 2026



Vehicle

400 V Kia EV3 model year 2025



Key components

EMR4 150 kW series with **ERA-based identification parameters**

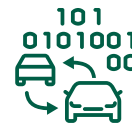


Set-up

Highlight: **“Rolling testbench”** in final vehicle environment

Full instrumentation for precise data acquisition:

- HV voltage & current sensors
- torque sensors in gearbox and drive shafts



Focus

Live data transfer with LTE realtime cloud logging device

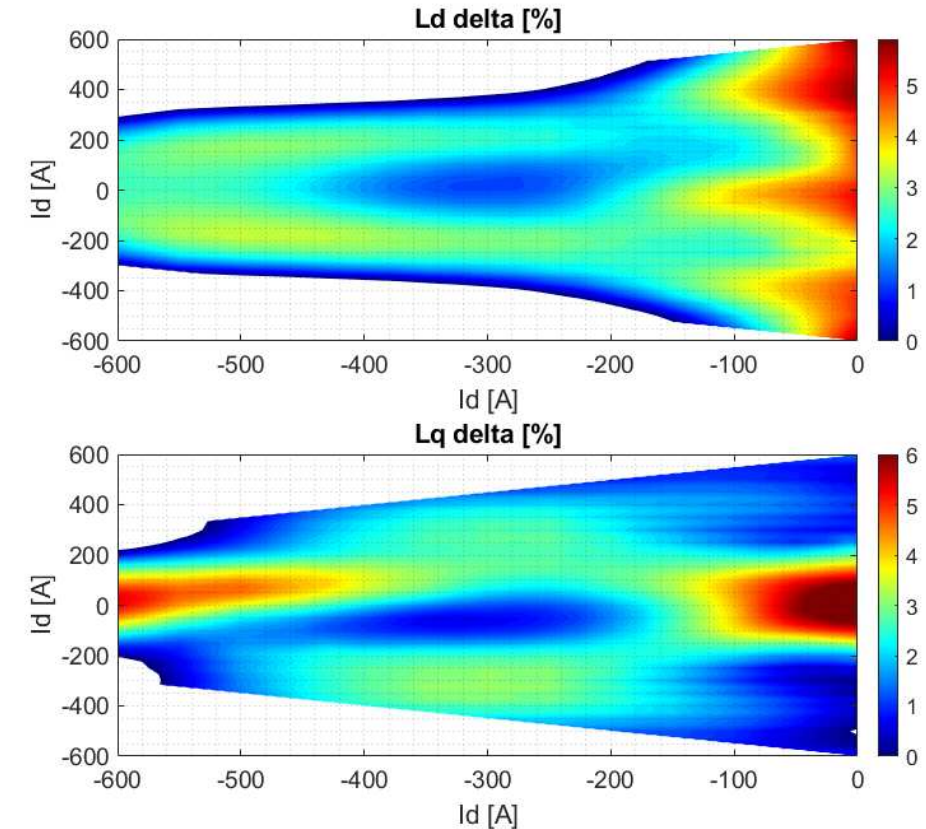
Generation of “Digital Twin” for 1-to-1 modelling of drive unit

Evaluations on vehicle level – Simulative assumptions

- Input data:
Measured parameters with identical EMR3 series motor
- PsiD and PsiQ scaled with delta (ERA vs. test bench) over Id and Iq:

$$\psi_{s,scaled}^{dq} = \psi_{s,orig}^{dq} \left(1 - \frac{L_{s,max}}{L_{s,SAG} - L_{s,ERA}} \right)$$

- EDS simulation done with related motor model



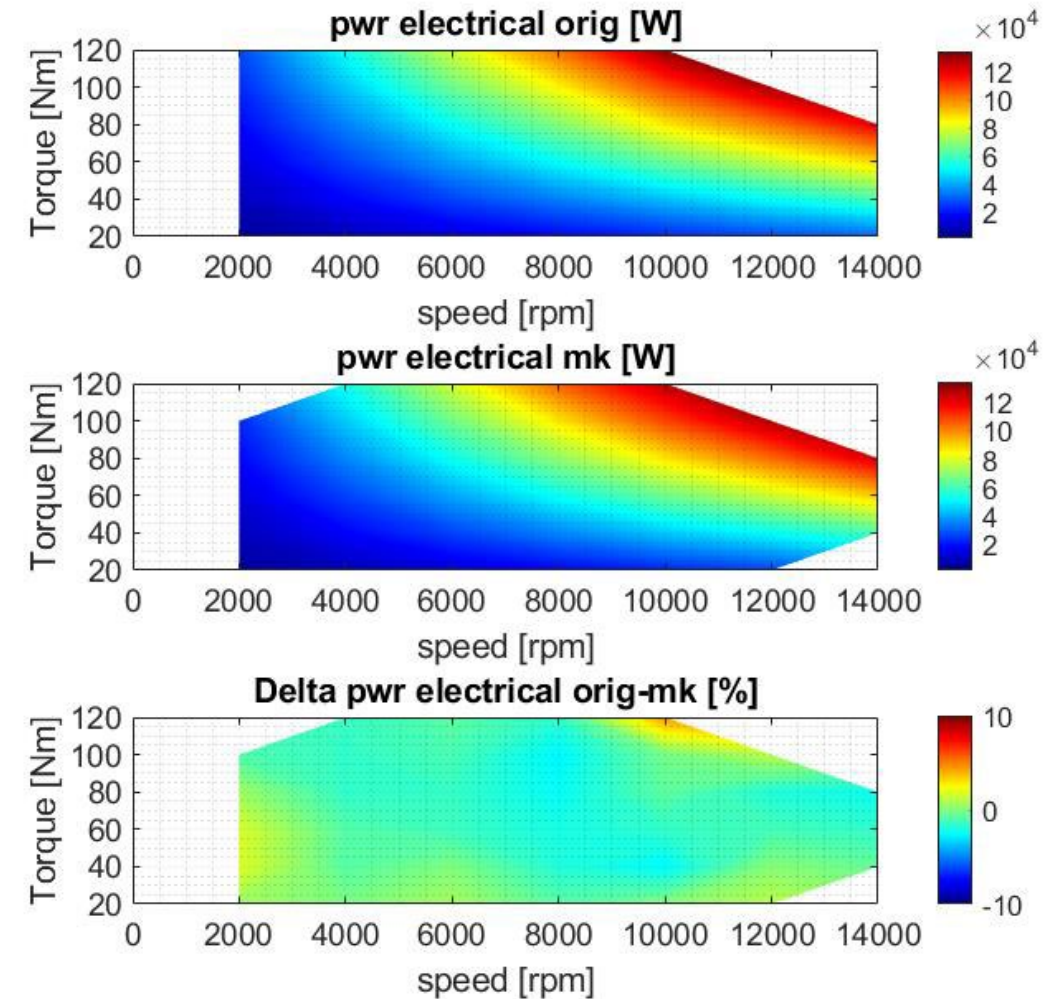
Approx. 2 % differences in total vehicle consumption (rough estimation)

Evaluations on vehicle level – Chassis dyno measurements

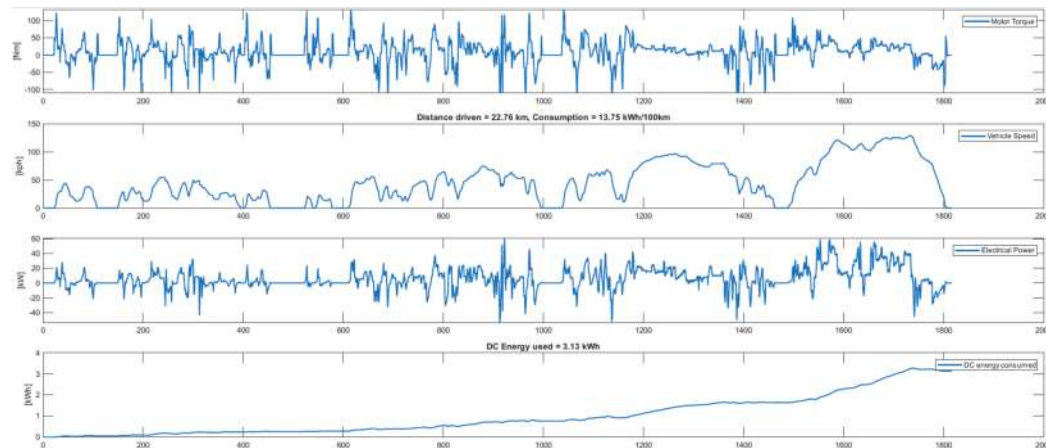
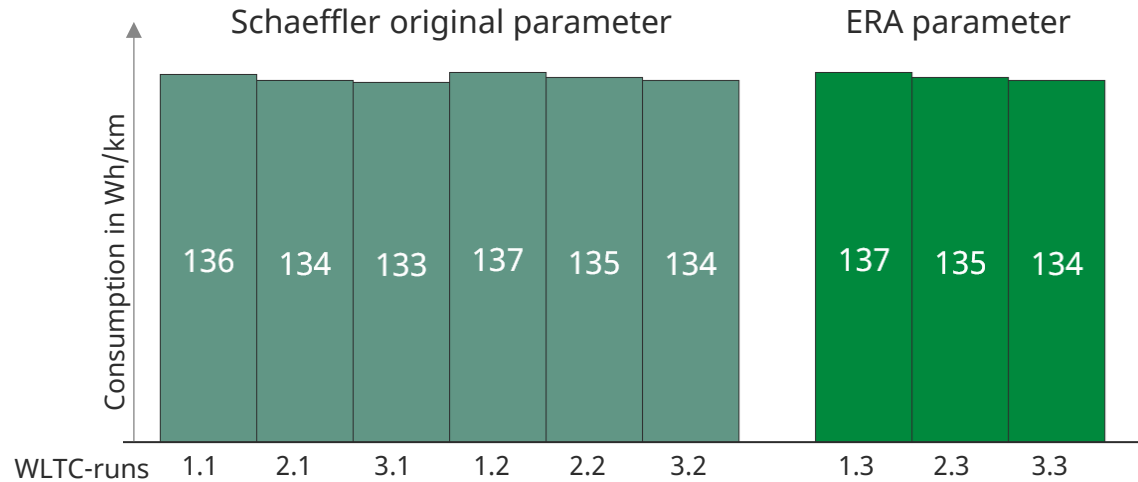
Driving scenario #1 with SC.EV32:

Constant drive with single torque and speed plateaus
(20 - 140 Nm and 2000 - 14000 rpm)

- Calculation on vehicle level
 - Averaging of plateaus
 - Integration into lookup tables
 - Calculation of electrical drivetrain power



Evaluations on vehicle level – Chassis dyno measurements



Driving scenario #2 with SC.EV32 :

Repeatable WLTCs (3 cycles in one block)

- 6x Schaeffler original parameter
- 3x ERA-based parameter
- Consumption decrease related to warming up reducer oil
→ less losses in reducer

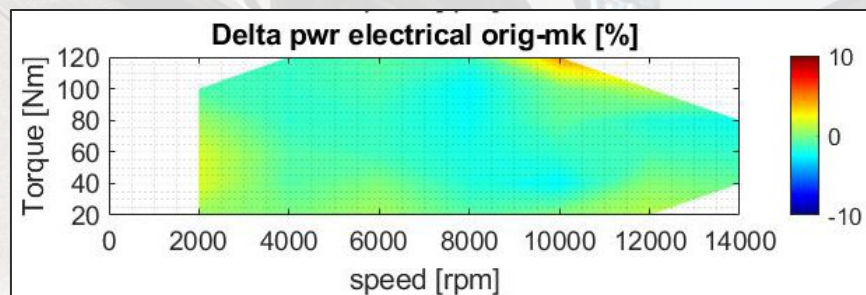
Evaluations on vehicle level – Chassis dyno measurements

Driving scenario #1 with SC.EV32 :

Constant drive with single torque and speed plateaus

(20 - 140 Nm and 2000 - 14000 rpm)

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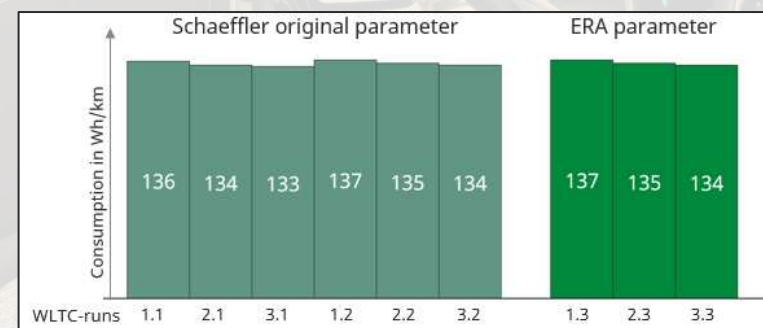


Constant drive: < 0.5 % deviation in all relevant WLTC areas

Driving scenario #2 with SC.EV32 :

Repeatable WLTCs (3 cycles in one block)

- 6x Schaeffler original parameter
- 3x ERA-based parameter
- Consumption decrease related to warming up reducer oil
 - less losses in reducer



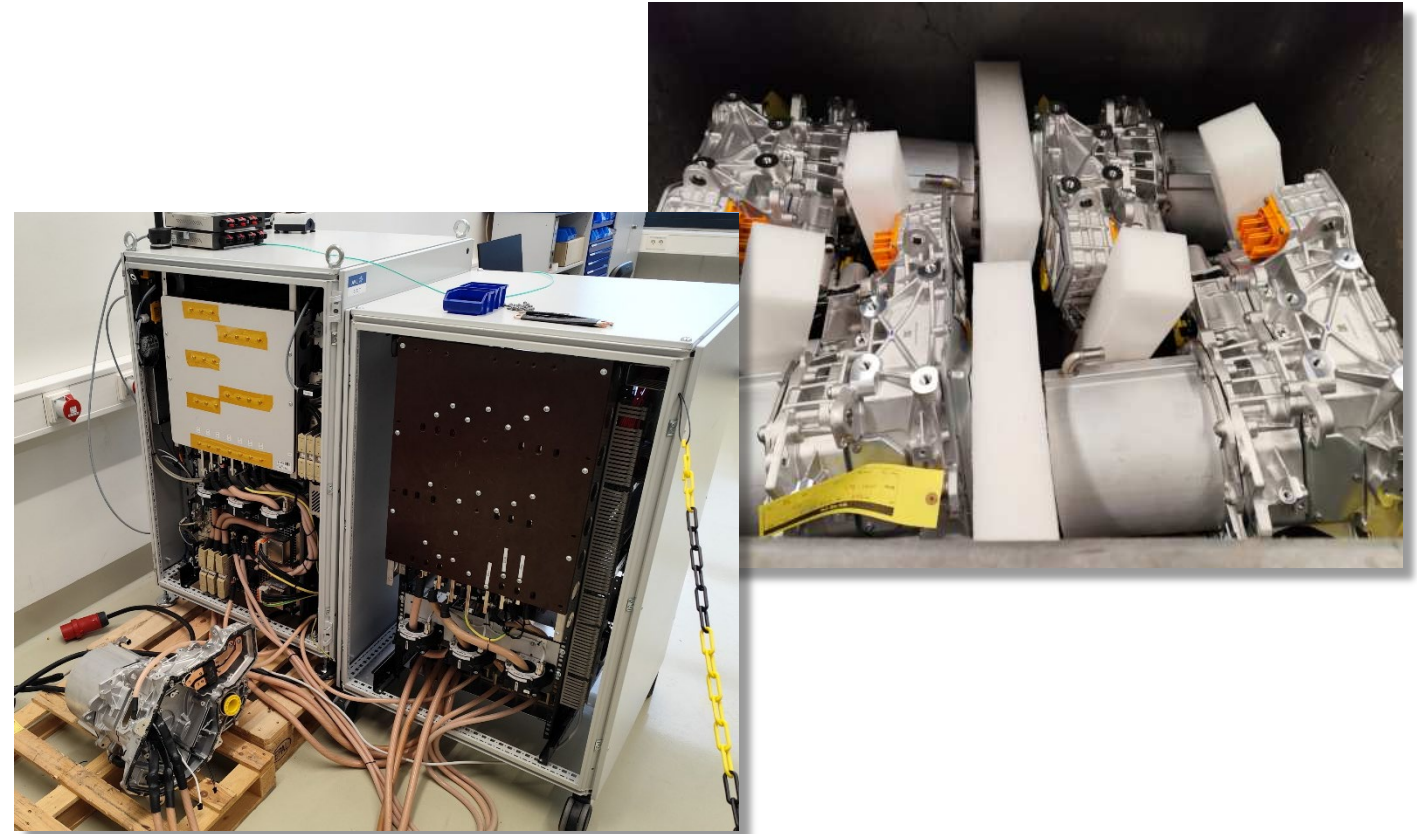
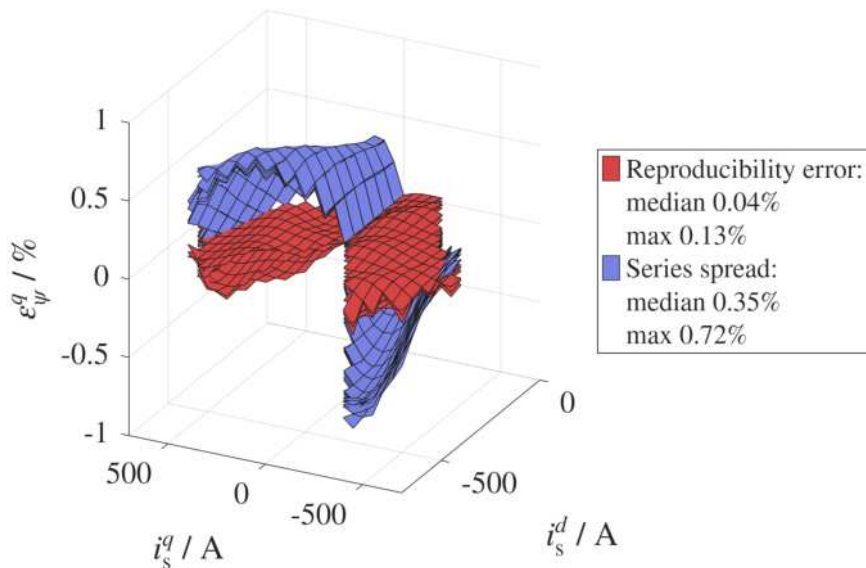
**Highly repeatable WLTC results: deviations < 0.5 %
- less than test-bench measurement uncertainty**

Series identification with ERA



Series identification with ERA on EMR4 series

- 15 Schaeffler EMR4 machines from 9 months of series production
 - Each machine individually identified
- Figure shows 2 machines, identified 4 consecutive times each, evaluated in MTPA area



**High reproducibility of ERA-based identification:
Series-production variation clearly identifiable**

Summary & Outlook



Summary and Outlook

Summary

- High reproducibility ($< 0,13 \%$)
- Cost dyno $\gg$ cost ERA (less hardware, fast procedure)
- Accuracy: $< 2,26 \%$ (dyno_{torque}), $< 0,42 \%$ (dyno_{efficiency}), $< 0,5 \%$ (vehicle_{WLTC})

Outlook

- Identification of parameter dependencies on angle, speed & iron losses
- Rotor-position-sensorless ERA
- Automated identification on ERA
- Use-cases: Failure analysis, EoL integration, new identification fields



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