

Internal model based grid state estimation

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Outline I

1 Internal model based grid state estimation



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- Introduction
- Internal model principle
- Observer design
- Implementation
- Conclusion



Introduction

Motivation: The future low-inertia power system—A likely guess [1]



- more distributed generation / renewable energy systems
- diminishing mechanical inertia
- hybrid grid and transmission topologies (e.g. AC & DC)
- more unbalanced faults (> 75% of faults already today)
- more loosely-coupled & unbalanced micro-grids
- more power electronics

⇒ Faster dynamics/transients, more harmonics & weaker overall grid!

⇒ Grid state estimation in real time crucial

⇒ ... for balancing, harmonics suppression, frequency/voltage support!

Introduction

Problem statement

For measured grid signal (voltage, current or power), given by

$$y(t) := a_0 + \sum_{\nu \in \mathbb{H}_n} \underbrace{a_\nu(t) \cos(\phi_\nu(t))}_{=: y_\nu(t)} \quad \text{where} \quad \begin{cases} \mathbb{H}_n := \{1, \nu_2, \dots, \nu_n\} \subset \mathbb{Q}_{>0} \\ \phi_\nu(t) := \int_0^t \nu \omega(\tau) d\tau + \phi_{\nu,0}, \end{cases} \quad (1)$$

the **main goals** are

- (i) signal estimation after *prescribed settling time* $t_{\text{set}} > 0$ s for some $\varepsilon_y > 0$, i.e.

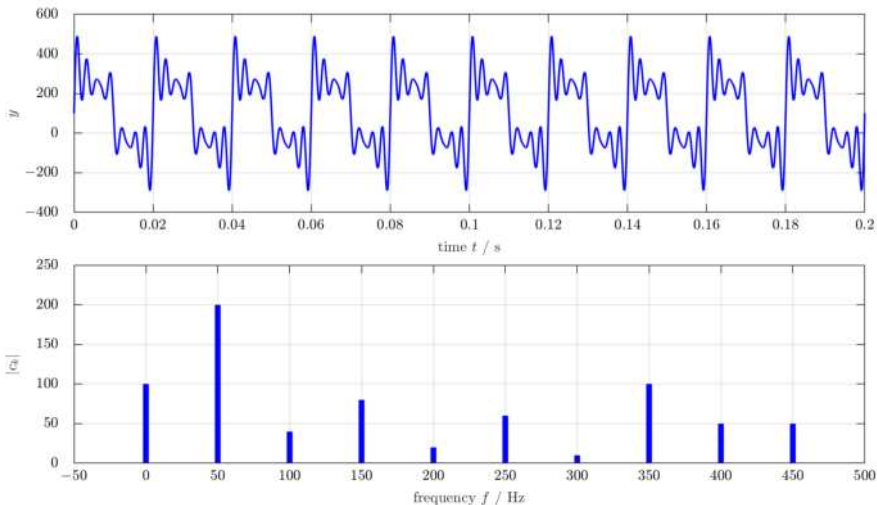
$$\forall t \geq t_{\text{set}} : |y(t) - \hat{y}(t)| \leq \varepsilon_y \quad \text{with} \quad \hat{y}(t) := \hat{a}_0 + \sum_{\nu \in \mathbb{H}_n} \underbrace{\hat{a}_\nu(t) \cos(\hat{\phi}_\nu(t))}_{=: \hat{y}_\nu(t)}; \quad (2)$$

- (ii) amplitude estimation, i.e. $\hat{a}_0 \rightarrow a_0$ and $\hat{a}_\nu \rightarrow a_\nu$ for all $\nu \in \mathbb{H}_n$; and

- (iii) frequency and angle estimation, i.e. $\hat{\omega} \rightarrow \omega$ and $\hat{\phi}_\nu \rightarrow \phi_\nu$ for all $\nu \in \mathbb{H}_n$.

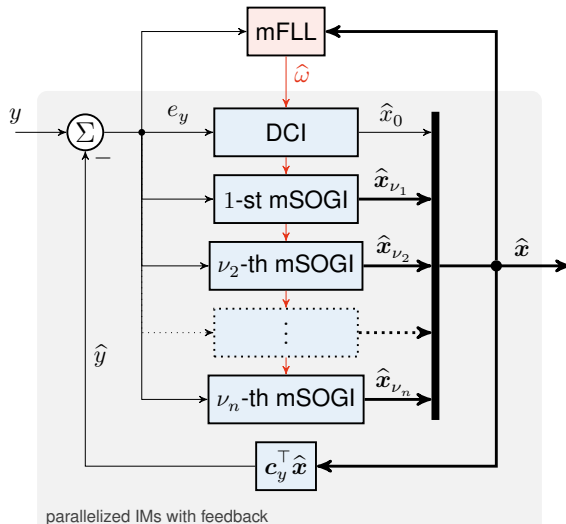
Introduction

Problem statement (illustration)



Introduction

Proposed solution: **Nonlinear observer** consisting of ...



- **DC-integrator (DCI)** for DC offset estimation
- **modified Second-Order-Generalized-Integrators (mSOGIs)** for harmonics estimation
- **modified frequency-locked loop (mFLL)** for frequency estimation

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Internal model principle

Motivation

Walter M. Wonham (1985):

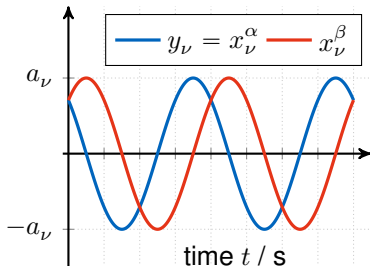
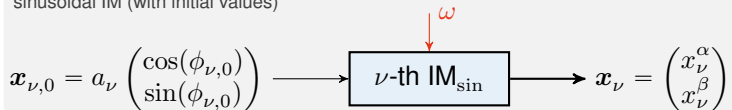
“Every good regulator [or observer] must incorporate a model of the outside world being capable to reduplicate the dynamic structure of the exogenous signals which the regulator [or observer] is required to process.” [2]



Internal model principle

Example: Sinusoidal signal reduplication of the ν -th harmonic where $\nu \in \mathbb{H}_n$

sinusoidal IM (with initial values)

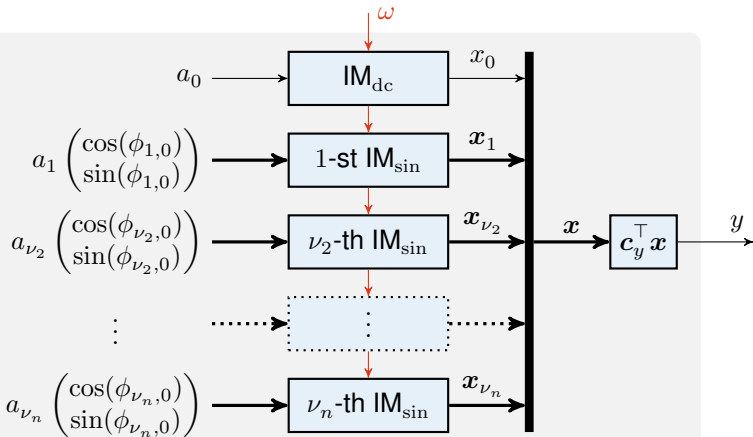


$$\frac{d}{dt} \mathbf{x}_{\nu} = \omega(t) \begin{bmatrix} 0 & -\nu \\ \nu & 0 \end{bmatrix} \mathbf{x}_{\nu}, \quad \mathbf{x}_{\nu}(0) = \mathbf{x}_{\nu,0}$$

$$y_{\nu} = \begin{pmatrix} 1 & 0 \end{pmatrix} \mathbf{x}_{\nu}$$

Internal model principle

Overall signal reduplication by parallelization of IMs



parallelized IMs (with initial values)

Internal model principle

Dynamics of parallelized IMs

$$\begin{aligned}
 \frac{d}{dt} \underbrace{\begin{pmatrix} x_0 \\ x_1^\alpha \\ x_1^\beta \\ x_1^\alpha \\ x_{\nu_2} \\ x_{\nu_2}^\beta \\ \vdots \\ x_{\nu_n}^\alpha \\ x_{\nu_n}^\beta \end{pmatrix}}_{=: \mathbf{x} \in \mathbb{R}^{2n+1}} &= \omega(t) \underbrace{\begin{bmatrix} 0 & & & & \\ & \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} & & & \\ & & \nu_2 \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} & & \\ & & & \ddots & \\ & & & & \nu_n \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \end{bmatrix}}_{=: \mathbf{A} \in \mathbb{R}^{(2n+1) \times (2n+1)}} \mathbf{x}, \quad \mathbf{x}(0) = \mathbf{x}_0 \\
 y &= \underbrace{(1, \quad (1, \quad 0), \quad (1, \quad 0), \quad \dots \quad (1, \quad 0))}_{=: \mathbf{c}_y^\top \in \mathbb{R}^{1 \times (2n+1)}} \mathbf{x}
 \end{aligned}$$

$\Rightarrow$ Observation problem of an **observable** system $\Rightarrow$ **Observer design**

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Observer design

Overall observer and pole placement: **parallelized internal models** with **feedback**

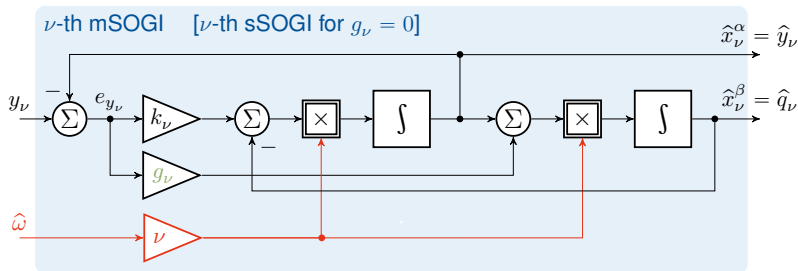
For $\mathbf{J} := \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}$ and $\mathbf{l}_\nu := \nu \begin{pmatrix} k_\nu \\ g_\nu \end{pmatrix}$, define the observer dynamics

$$\begin{aligned} \underbrace{\frac{d}{dt} \begin{pmatrix} \hat{x}_0 \\ \hat{x}_1 \\ \hat{x}_{\nu_2} \\ \vdots \\ \hat{x}_{\nu_n} \end{pmatrix}}_{=: \hat{\mathbf{x}} \in \mathbb{R}^{2n+1}} &= \hat{\omega}(t) \underbrace{\begin{bmatrix} \overset{0}{\mathbf{J}} & & & \\ & \nu_2 \mathbf{J} & & \\ & & \ddots & \\ & & & \nu_n \mathbf{J} \end{bmatrix}}_{=: \mathbf{A} - \mathbf{l} \mathbf{c}_y^\top =: \mathbf{H}} - \underbrace{\begin{pmatrix} l_0 \\ l_1 \\ l_{\nu_2} \\ \vdots \\ l_{\nu_n} \end{pmatrix} \mathbf{c}_y^\top}_{\mathbf{l} \mathbf{c}_y^\top} \hat{\mathbf{x}} - \hat{\omega}(t) \mathbf{l} y, \quad \hat{\mathbf{x}}(0) = \hat{\mathbf{x}}_0 \\ \hat{y} &= \underbrace{(1, \quad (1, \quad 0), \quad (1, \quad 0), \quad \dots \quad (1, \quad 0))}_{=: \mathbf{c}_y^\top \in \mathbb{R}^{1 \times (2n+1)}} \hat{\mathbf{x}} \end{aligned}$$

- Recall: $(\mathbf{c}_y^\top, \mathbf{A})$ observable $\implies \exists \mathbf{l} \in \mathbb{R}^{2n+1}: \mathbf{H} := \mathbf{A} - \mathbf{l} \mathbf{c}_y^\top$ Hurwitz!
- Pole placement: $\mathbf{l} = \mathbf{S} \mathbf{p}_H^* \implies s_0^* = -p_0^* \wedge \forall \nu \in \mathbb{H}_n: s_{\nu,1/2}^* = -p_\nu^* \pm j\nu$

Observer design

Modified SOGI (mSOGI) for ν -th harmonic estimation: ν -th IM_{sin} with extended feedback

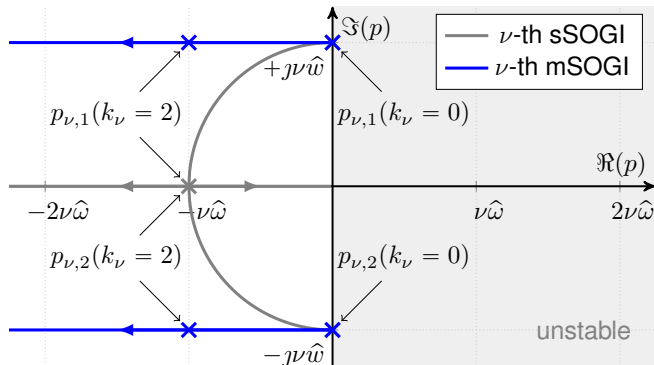


$$\frac{d}{dt} \hat{\mathbf{x}}_\nu(t) = \hat{\omega}(t) \underbrace{\begin{bmatrix} -\nu k_\nu & -\nu \\ \nu - \nu g_\nu & 0 \end{bmatrix}}_{=: \mathbf{A}_\nu - \mathbf{l}_\nu(k_\nu, g_\nu) \mathbf{c}_y^\top} \hat{\mathbf{x}}_\nu(t) + \hat{\omega}(t) \underbrace{\begin{pmatrix} \nu k_\nu \\ \nu g_\nu \end{pmatrix}}_{=: \mathbf{l}_\nu(k_\nu, g_\nu)} y_\nu(t), \quad \hat{\mathbf{x}}_\nu(0) = \hat{\mathbf{x}}_{\nu,0}$$

$$\hat{y}_\nu(t) = \mathbf{c}_\nu^\top \hat{\mathbf{x}}_\nu(t)$$

Observer design

Comparison of root loci of ν -th sSOGI and mSOGI



sSOGI

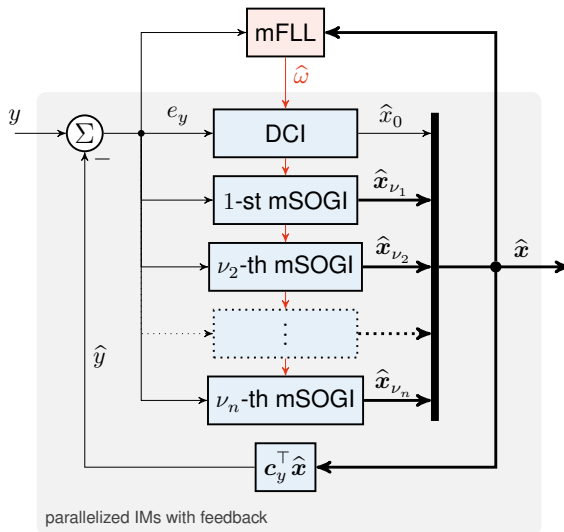
$$p_{\nu,1/2} = -\frac{\nu\hat{\omega}k_\nu}{2} \left(1 \pm \sqrt{1 - \frac{4}{k_\nu^2}} \right)$$

mSOGI (for $g_\nu = -\frac{k_\nu^2}{4}$)

$$p_{\nu,1/2} = -\frac{\nu\hat{\omega}k_\nu}{2} \pm j\nu\hat{\omega}.$$

Observer design

Overall observer structure



Outline I

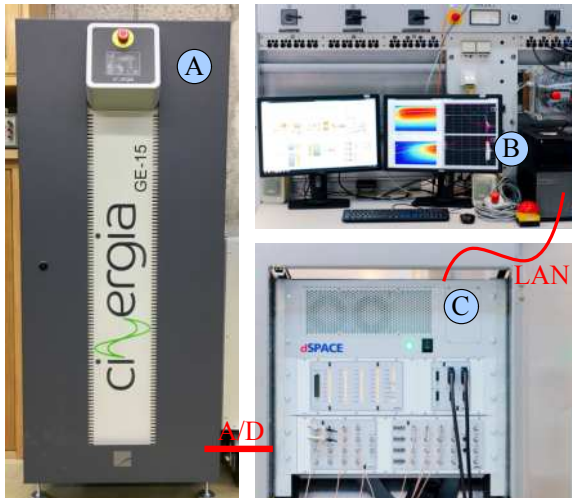
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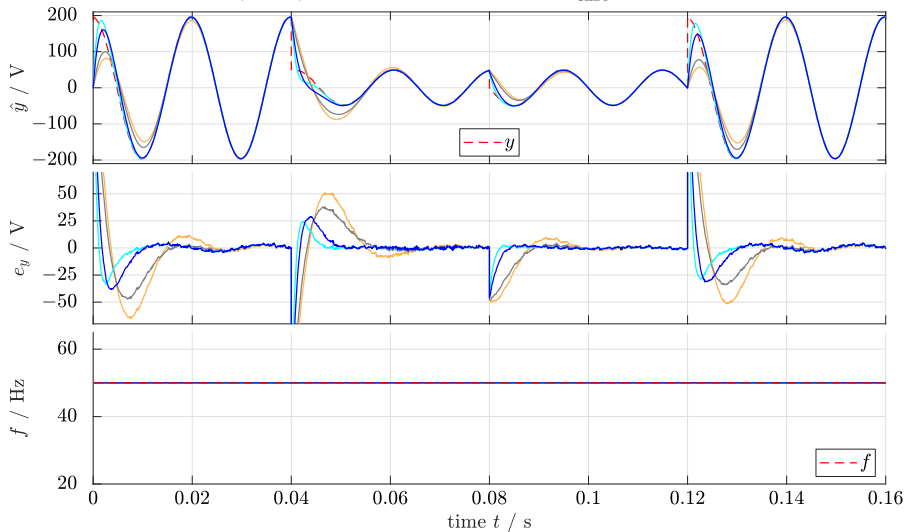
Implementation

Laboratory setup: (A) Grid emulator, (B) Host-PC and (C) Real-time system



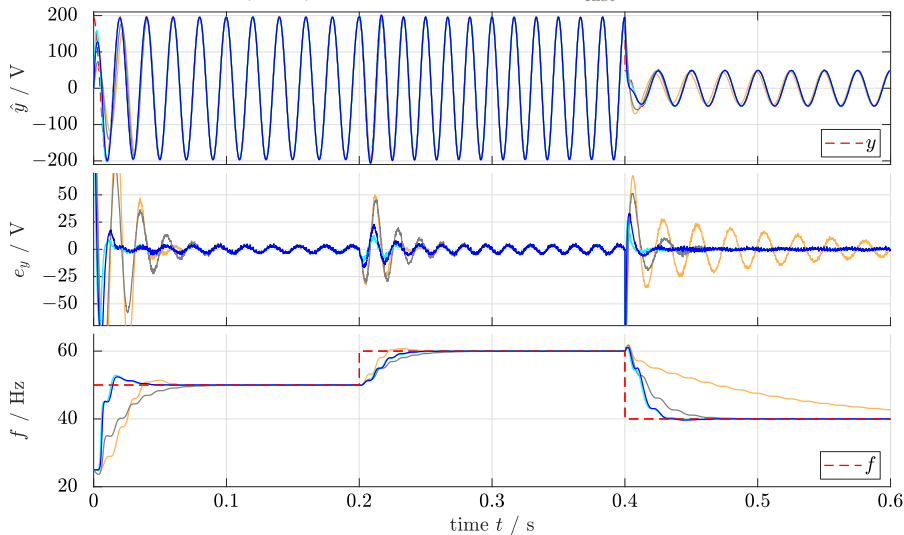
Implementation

Measurements w/o FLL ($\nu = 1$): — mSOGI, — mSOGI_{fast}, — sSOGI & — ANF



Implementation

Measurements **with** FLL ($\nu = 1$): — mSOGI, — mSOGI_{fast}, — sSOGI & — ANF



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Conclusion

Summary and outlook

To take home

- **unified theory** for grid state estimation, based on
 - **internal model principle** and **parallelization** $\implies$ observation problem;
 - **parallelized internal models** with **feedback** (mSOGIs) $\implies$ modular structure;
 - **pole placement** $\implies$ prescribed settling time
 - **modified** frequency-locked loop (FLL) with sign-correct anti-windup and rate limitation
- **real-time estimation**
- **positive, negative** and **zero sequence extraction** for each harmonic (also possible)

Future work

- Frequency Locked-Loop weakest component $\implies$ further improvement
- Reduction of noise sensitivity $\implies$ (extended) Kalman filter design or pre-filtering?
- three-phase implementation, validation and test in laboratory

