

Grid state estimation: An internal model based approach

Habilitationsvortrag im Rahmen der Schlussbewertung

Christoph Hackl

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Technical University of Munich

Outline I

1 Teaching and research activities

2 Grid state estimation: An internal model based approach

Outline I

1 Teaching and research activities

- Teaching
- Research group
- Research projects
- Publications

Outline I

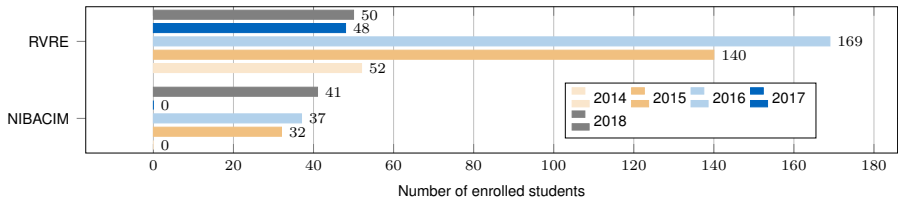
1 Teaching and research activities

■ Teaching

- Research group
- Research projects
- Publications

Teaching and research activities (2014-2018)

Teaching: Lectures, tutorials, practical courses and miscellaneous (3-6 SWS per semester)



■ Lectures, tutorials, practical courses & student projects

- “Regelung von regenerativen Energiesystemen” (WS, 3SWS with PhD students)
- “Non-identifier based adaptive control in mechatronics” (SS, 4SWS)
- “Projektstudium Antriebstechnik” [1–3] (Umsetzung EOF Lehrpreis, WS1415): **13**
- Supervised student projects: **>30** (master & bachelor thesis, seminars, internships)
- 3 lectures and 2 practical courses at Munich University of Applied Sciences: **>100**

■ Miscellaneous (e.g.)

- Winter School “Holistic Modeling & Control of Energy Systems”: **47** (w. Dörfler & Jokić)
- H2020 ITN Workshop “Electrical Drives and Predictive Control”: **15** (with M. Diehl)
- Industrial training on “Optimal feedforward torque control of anisotropic synchronous machines”, Volkswagen, Salzgitter: **8**
- Invited lecture on “Modeling and control of renewable energy systems” and seminar on “Selected topics in energy research”, CREATE, Singapore (May-July 2017): **10-20**

Outline I

1 Teaching and research activities

- Teaching
- Research group
- Research projects
- Publications

Teaching and research activities (2014-2018)

Research group: 9 PhD candidates, 1 Post-Doc, several PhD collaborations@EAL&NES



H. Eldeeb, M.Sc.
(CRES, 09/2015)



C. Dirscherl, M.Sc.
(CRES, 01/2014)



C. Hackl, Dr.-Ing.
(CRES, 01/2014)



J. Kullick, M.Sc.
(CRES, 10/2015)



K. Schechner, M.Sc.
(CRES, 01/2014)



C. Ladisla, M.Sc.
(CRES, 01/2018)

External PhD students



M. Landerer, M.Sc.
(CRES, 06/2016)



Z. Zhang, Dr.-Ing.
(CRES/EAL, 07/2015)



K. Bär, M.Sc.
(THI, 07/2017)



A. Birda, M.Sc.
(BMW, 04/2016)



S. Krüner, M.Sc.
(SINNPower, 11/2015)

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Outline I

1 Teaching and research activities

- Teaching
- Research group
- **Research projects**
- Publications

Teaching and research activities (2014-2018)

Research projects with focus on **modeling, simulation, control, efficiency** and **reliability**
(funding: > 2.2 million €; e.g. DAAD, Bavaria, BMBF, BMWi, DFG, EU)

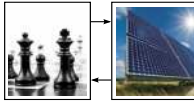
Large-scale WTS



Small-scale WTS



MPC for RES



AWE systems



Geothermal energy



Wave energy (SinnPower)



Electric vehicles (BMW)



Power systems



Biogas power plants



Multi-level converters



Outline I

1 Teaching and research activities

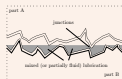
- Teaching
- Research group
- Research projects
- Publications

Teaching and research activities (2014-2018)

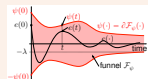
Publications (1 monograph, 6 chapters, 21 articles & 49 conference papers; all peer-reviewed)



System identification
[12–16]



Friction
[17, 18]



Non-identifier based adaptive control
[17, 19–30], [31–34]



Paper coating machines
[7–11]



Teaching [117, 118], [1–3, 34, 119–121, 121, 122]



Robotics & Mechatronics [17, 35–44], [18, 34, 45]



Electro-active polymers
[4–6]

Mechatronic & renewable energy systems



Power electronics
[46, 47], [48–56], [57–63], [34, 64–69], [70–75], [76]



Renewable energy systems [47], [16, 31, 33, 34, 48, 51, 55, 56, 58–60, 62, 64, 70, 75, 76, 81–83, 86, 88, 95, 100–116]



Electrical drives (motors/generators)
[17, 19, 21, 22, 40, 44, 77–80], [16, 32, 34, 57, 65, 70, 72, 75, 81–99]

Outline I

2 Grid state estimation: An internal model based approach

- Introduction
- Internal model principle
- Observer design
- Frequency estimation
- Harmonic sequence extraction
- Conclusion

Outline I

2 Grid state estimation: An internal model based approach

■ Introduction

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Introduction

Motivation: The future power system—A likely guess



- more distributed generation / renewable energy systems
- diminishing mechanical inertia
- hybrid grid and transmission topologies (e.g. AC & DC)
- more unbalanced faults ($> 75\%$ of faults already today)
- more loosely-coupled & unbalanced micro-grids
- more power electronics

⇒ Faster dynamics/transients, more harmonics & weaker overall grid!

⇒ Grid state estimation in real time crucial

⇒ ... for balancing, harmonics suppression, frequency/voltage support!

Introduction

Problem statement

For measured grid signal (voltage, current or power), given by

$$y(t) := a_0 + \sum_{\nu \in \mathbb{H}_n} \underbrace{a_\nu(t) \cos(\phi_\nu(t))}_{=: y_\nu(t)} \quad \text{where} \quad \begin{cases} \mathbb{H}_n := \{1, \nu_2, \dots, \nu_n\} \subset \mathbb{Q}_{>0} \\ \phi_\nu(t) := \int_0^t \nu \omega(\tau) d\tau + \phi_{\nu,0}, \end{cases} \quad (1)$$

the **main goals** are

- (i) signal estimation after *prescribed settling time* $t_{\text{set}} > 0$ s for some $\varepsilon_y > 0$, i.e.

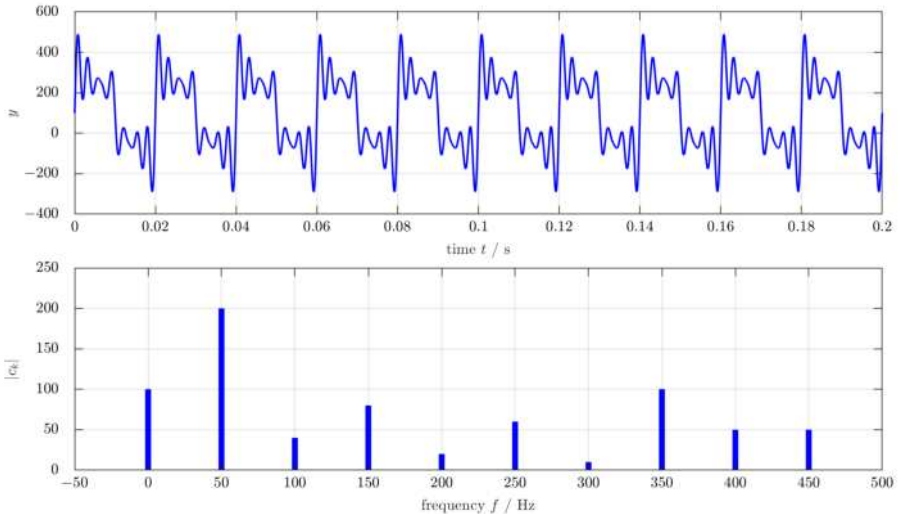
$$\forall t \geq t_{\text{set}}: |y(t) - \hat{y}(t)| \leq \varepsilon_y \quad \text{with} \quad \hat{y}(t) := \hat{a}_0 + \sum_{\nu \in \mathbb{H}_n} \underbrace{\hat{a}_\nu(t) \cos(\hat{\phi}_\nu(t))}_{=: \hat{y}_\nu(t)}; \quad (2)$$

- (ii) amplitude estimation, i.e. $\hat{a}_0 \rightarrow a_0$ and $\hat{a}_\nu \rightarrow a_\nu$ for all $\nu \in \mathbb{H}_n$; and

- (iii) frequency and angle estimation, i.e. $\hat{\omega} \rightarrow \omega$ and $\hat{\phi}_\nu \rightarrow \phi_\nu$ for all $\nu \in \mathbb{H}_n$.

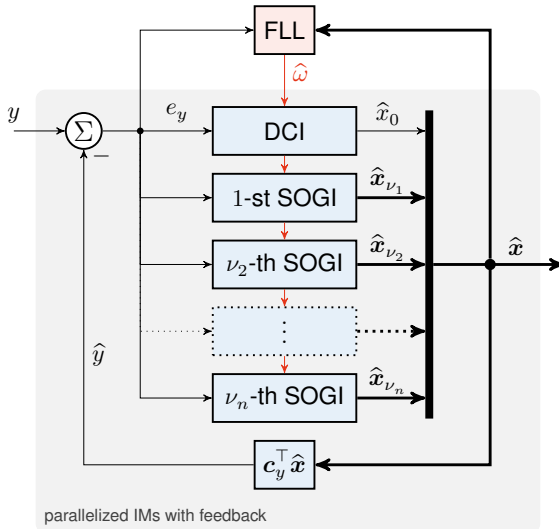
Introduction

Problem statement (illustration)



Introduction

Proposed solution: Time-varying observer consisting of parallelized IMs with feedback and FLL



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Internal model principle

Motivation

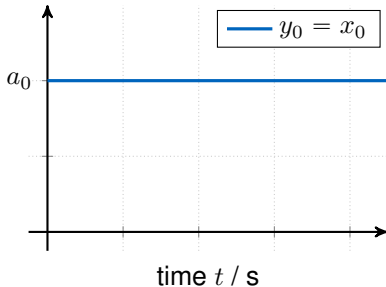
Francis Wonham (1985):

“Every good regulator [or observer] must incorporate a model of the outside world being capable to reduplicate the dynamic structure of the exogenous signals which the regulator [or observer] is required to process.” [123]

Internal model principle

Constant signal reduplication

constant IM (with initial value)



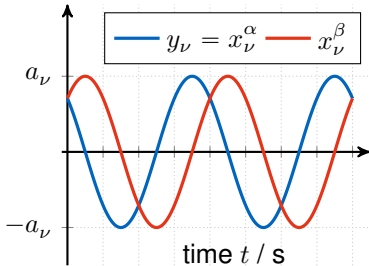
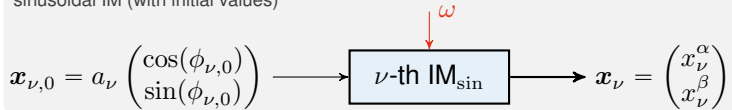
$$\frac{d}{dt}x_0 = 0, \quad x_0(0) = x_{0,0}$$

$$y_0 = x_0$$

Internal model principle

Sinusoidal signal reduplication of the ν -th harmonic where $\nu \in \mathbb{H}_n$

sinusoidal IM (with initial values)

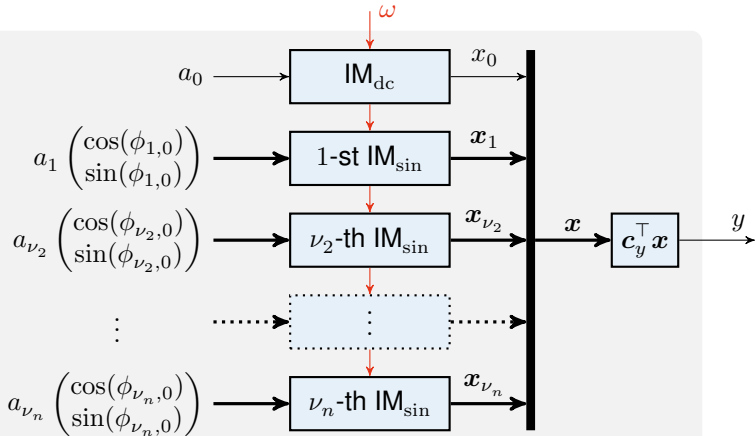


$$\frac{d}{dt} \mathbf{x}_{\nu} = \omega(t) \begin{bmatrix} 0 & -\nu \\ \nu & 0 \end{bmatrix} \mathbf{x}_{\nu}, \quad \mathbf{x}_{\nu}(0) = \mathbf{x}_{\nu,0}$$

$$y_{\nu} = (1, 0) \mathbf{x}_{\nu}$$

Internal model principle

Overall signal reduplication by parallelization of IMs



parallelized IMs (with initial values)

Internal model principle

Dynamics of parallelized IMs

$$\begin{aligned}
 \underbrace{\frac{d}{dt} \begin{pmatrix} x_0 \\ \begin{pmatrix} x_1 \\ x_1^\beta \end{pmatrix} \\ \begin{pmatrix} x_{\nu_2} \\ x_{\nu_2}^\beta \end{pmatrix} \\ \vdots \\ \begin{pmatrix} x_{\nu_n} \\ x_{\nu_n}^\beta \end{pmatrix} \end{pmatrix}}_{=: \mathbf{x} \in \mathbb{R}^{2n+1}} &= \omega(t) \underbrace{\begin{bmatrix} 0 & & & & \\ & \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} & & & \\ & & \nu_2 \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} & & \\ & & & \ddots & \\ & & & & \nu_n \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \end{bmatrix}}_{=: \mathbf{A} \in \mathbb{R}^{(2n+1) \times (2n+1)}} \mathbf{x}, \quad \mathbf{x}(0) = \mathbf{x}_0 \\
 y &= \underbrace{(1, \quad (1, \quad 0), \quad (1, \quad 0), \quad \dots \quad (1, \quad 0))}_{=: \mathbf{c}_y^\top \in \mathbb{R}^{1 \times (2n+1)}} \mathbf{x}
 \end{aligned}$$

⇒ Observation problem of a dynamical system ... if observable!

Internal model principle

Observability of parallelized IMs (for constant $\omega > 0$)

$$\begin{aligned}
 \text{rank} \begin{bmatrix} c_y^\top \\ c_y^\top A \\ c_y^\top A^2 \\ c_y^\top A^3 \\ c_y^\top A^4 \\ \vdots \\ c_y^\top A^{2n-1} \\ c_y^\top A^{2n} \end{bmatrix} &= \\
 \text{rank} \begin{bmatrix} 1 & 1 & 0 & 1 & 0 & \dots & 1 & 0 \\ 0 & 0 & -1 & 0 & -\nu_2^2 & \dots & 0 & -\nu_n^2 \\ 0 & -1 & 0 & -\nu_2^2 & 0 & \dots & -\nu_n^2 & 0 \\ 0 & 0 & 1 & 0 & \nu_2^3 & \dots & 0 & \nu_n^3 \\ 0 & 1 & 0 & \nu_2^4 & 0 & \dots & \nu_n^4 & 0 \\ 0 & \vdots & & \vdots & & & & \vdots \\ 0 & 0 & (-1)^n & 0 & (-1)^n \nu_2^{2n-1} & \dots & 0 & (-1)^n \nu_n^{2n-1} \\ 0 & (-1)^n & 0 & (-1)^n \nu_2^{2n} & 0 & \dots & (-1)^n \nu_n^{2n} & 0 \end{bmatrix} \\
 &= 2n + 1 \iff \nu_i \neq \nu_j \text{ for all } i, j \in \{1, \dots, n\}
 \end{aligned}$$

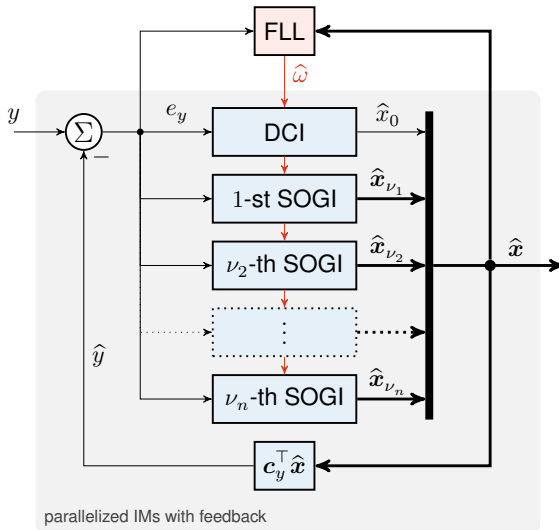
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- **Observer design**
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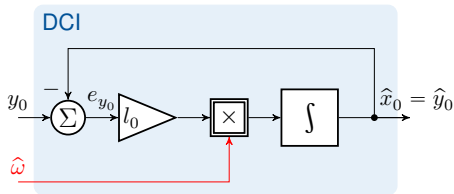
Observer design

Overall observer structure



Observer design

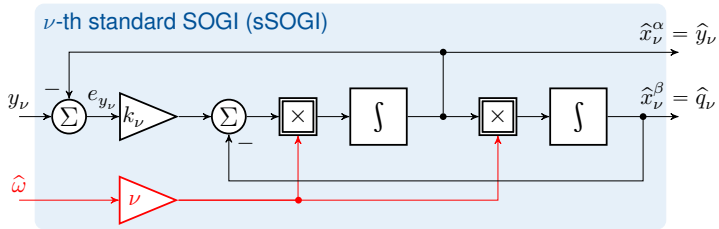
DC-Integrator (DCI) for constant signal estimation: IM_{dc} with **feedback**



$$\begin{aligned} \frac{d}{dt} \hat{x}_0 &= -\hat{\omega}(t) l_0 \hat{x}_0 + \hat{\omega}(t) l_0 y_0, & \hat{x}_0(0) &= 0 \\ \hat{y}_0 &= \hat{x}_0 \end{aligned}$$

Observer design

Standard SOGI (sSOGI) for ν -th harmonic estimation: ν -th IM_{sin} with feedback

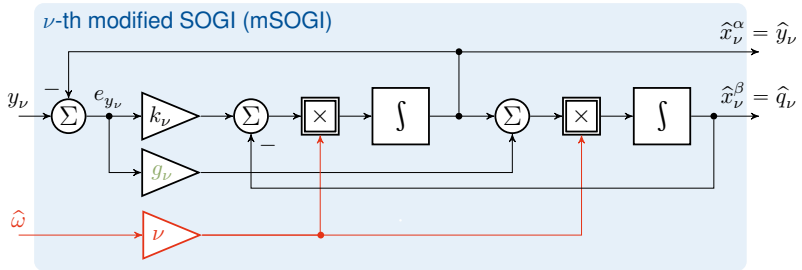


$$\begin{aligned} \frac{d}{dt} \underbrace{\begin{pmatrix} \hat{x}_\nu^\alpha(t) \\ \hat{x}_\nu^\beta(t) \end{pmatrix}}_{=: \hat{\mathbf{x}}_\nu(t) \in \mathbb{R}^2} &= \underbrace{\hat{\omega}(t)}_{=: \mathbf{A}_\nu - \mathbf{l}_\nu(k_\nu) \mathbf{c}_y^\top} \begin{bmatrix} 0 & -\nu \\ \nu & 0 \end{bmatrix} \hat{\mathbf{x}}_\nu(t) + \underbrace{\hat{\omega}(t)}_{=: \mathbf{l}_\nu(k_\nu)} \underbrace{\begin{pmatrix} \nu k_\nu \\ 0 \end{pmatrix}}_{=: \mathbf{l}_\nu(k_\nu)} y_\nu(t), \quad \hat{\mathbf{x}}_\nu(0) = \hat{\mathbf{x}}_{\nu,0} \end{aligned}$$

$$\hat{y}_\nu(t) = \underbrace{\begin{pmatrix} 1 & 0 \end{pmatrix}}_{=: \mathbf{c}_\nu^\top \in \mathbb{R}^{1 \times 2}} \hat{\mathbf{x}}_\nu(t)$$

Observer design

Modified SOGI (mSOGI) for ν -th harmonic estimation: ν -th IM_{sin} with extended feedback

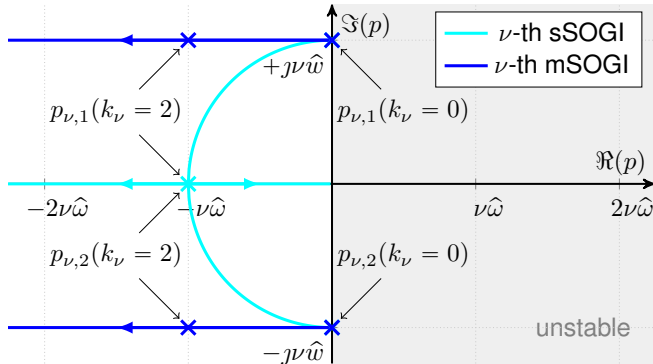


$$\frac{d}{dt} \hat{\mathbf{x}}_\nu(t) = \hat{\omega}(t) \underbrace{\begin{bmatrix} -\nu k_\nu & -\nu \\ \nu - \nu g_\nu & 0 \end{bmatrix}}_{=: \mathbf{A}_\nu - \mathbf{l}_\nu(k_\nu) \mathbf{c}_y^\top} \hat{\mathbf{x}}_\nu(t) + \hat{\omega}(t) \underbrace{\begin{pmatrix} \nu k_\nu \\ \nu g_\nu \end{pmatrix}}_{=: \mathbf{l}_\nu(k_\nu, g_\nu)} y_\nu(t), \quad \hat{\mathbf{x}}_\nu(0) = \hat{\mathbf{x}}_{\nu,0}$$

$$\hat{y}_\nu(t) = \mathbf{c}_\nu^\top \hat{\mathbf{x}}_\nu(t)$$

Observer design

Comparison of root loci of ν -th sSOGI and mSOGI



sSOGI

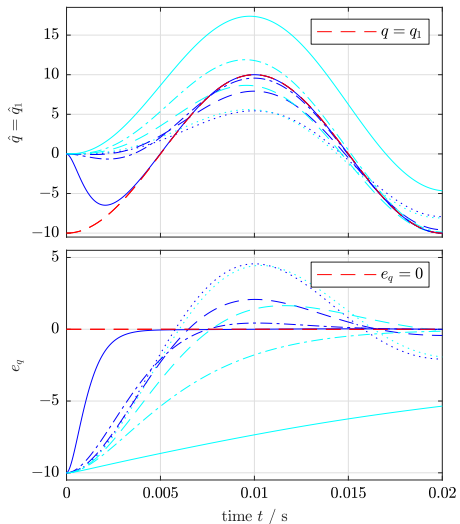
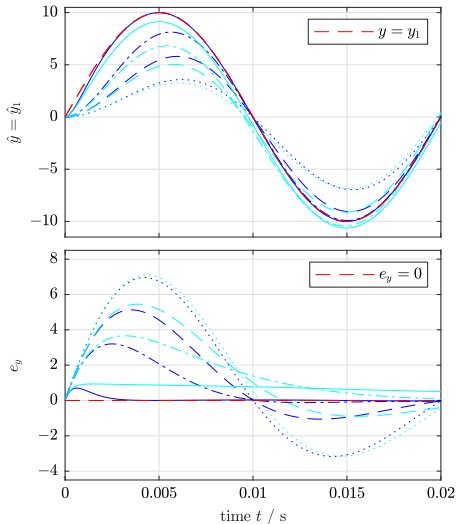
$$p_{\nu,1/2} = -\frac{\nu\hat{\omega}k_\nu}{2} \left(1 \pm \sqrt{1 - \frac{4}{k_\nu^2}} \right)$$

mSOGI (for $g_\nu = -\frac{k_\nu^2}{4}$)

$$p_{\nu,1/2} = -\frac{\nu\hat{\omega}k_\nu}{2} \pm j\nu\hat{\omega}.$$

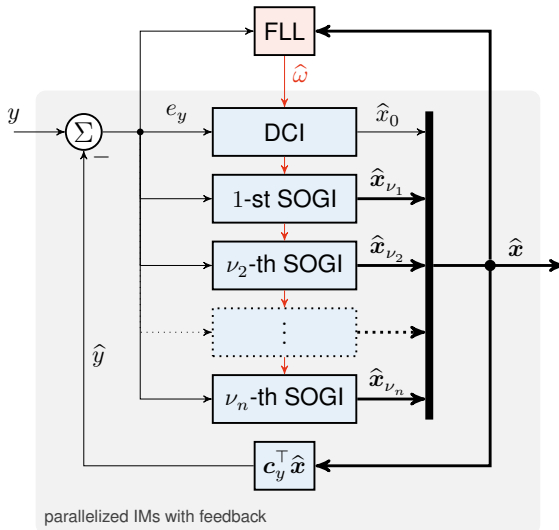
Observer design

Estimation performances of sSOGI (—) and mSOGI (—) for different $k_1 \in \{0.5, 1, 2, 10\}$



Observer design

Pole placement for overall observer



Observer design

Pole placement for overall observer: parallelized internal models with feedback

For $J := \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}$ and $l_\nu := \nu \begin{pmatrix} k_\nu \\ g_\nu \end{pmatrix}$, define the observer dynamics

$$\begin{aligned}
 & \stackrel{=: \hat{\mathbf{x}} \in \mathbb{R}^{2n+1}}{\frac{d}{dt} \begin{pmatrix} \hat{x}_0 \\ \hat{x}_1 \\ \hat{x}_{\nu_2} \\ \vdots \\ \hat{x}_{\nu_n} \end{pmatrix}} = \hat{\omega}(t) \overbrace{\begin{bmatrix} 0 & & & \\ & J & & \\ & & \nu_2 J & \\ & & & \ddots \\ & & & & \nu_n J \end{bmatrix}}^{=: A - l c_y^\top =: H} - \begin{pmatrix} l_0 \\ l_1 \\ l_{\nu_2} \\ \vdots \\ l_{\nu_n} \end{pmatrix} c_y^\top \hat{\mathbf{x}} - \hat{\omega}(t) l y, \quad \hat{\mathbf{x}}(0) = \hat{\mathbf{x}}_0 \\
 & \hat{y} = \underbrace{\begin{pmatrix} 1, & (1, & 0), & (1, & 0), & \dots & (1, & 0) \end{pmatrix}}_{=: c_y^\top \in \mathbb{R}^{1 \times (2n+1)}} \hat{\mathbf{x}}
 \end{aligned}$$

- Recall: $(c_y^\top, A)$ observable $\implies \exists l \in \mathbb{R}^{2n+1}: H := A - l c_y^\top$ Hurwitz!
- Pole placement: $l = S p_H^* \implies s_0^* = -p_0^* \wedge \forall \nu \in \mathbb{H}_n: s_{\nu,1/2}^* = -p_\nu^* \pm j\nu$

Observer design

Stability analysis for $\omega(\cdot) \in \mathcal{PC} \cap \mathcal{L}^\infty(\mathbb{R}_{\geq 0}; \mathbb{R}_{\geq \varepsilon})$ and $\hat{\omega}(\cdot) \in \mathcal{C}^1 \cap \mathcal{L}^\infty(\mathbb{R}_{\geq 0}; \mathbb{R}_{\geq \varepsilon})$

■ **Error dynamics** $e_x := x - \hat{x}$ and $e_\omega := \omega - \hat{\omega} \implies \frac{d}{dt} e_x = f(e_x, e_\omega, \dots)$

■ **Lyapunov candidate** $V(e_x) := e_x^\top P e_x$ and using

□ $H := A - l c_y^\top$ Hurwitz $\implies$

$\forall Q = Q^\top > 0 \exists P = P^\top > 0: H^\top P + P H = -Q < 0$ [124, Cor. 3.3.47]

□ $\forall a, b, m \in \mathbb{R}: 2ab = \frac{a^2}{m} + mb^2 - \left(\frac{a}{\sqrt{m}} - \sqrt{m}b\right)^2 \leq \frac{a^2}{m} + mb^2$

$\implies \frac{d}{dt} V(e_x) = \dots \leq -\mu_V V(e_x) + c_\omega e_\omega^2$ with $e_\omega(\cdot) \in \mathcal{L}^\infty(\mathbb{R}_{\geq 0}; \mathbb{R})$

□ Bellmann-Gronwall Lemma [34, Lemma 5.50]

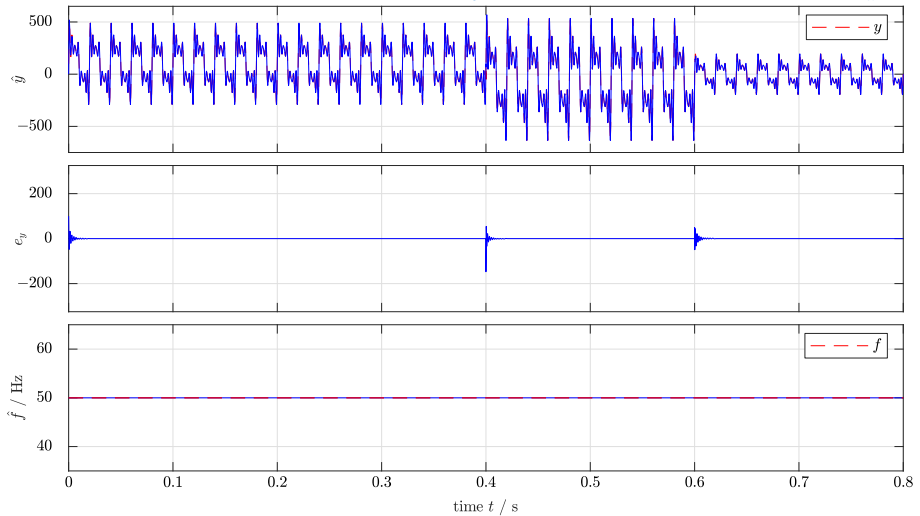
$\implies \forall t \geq t_i: V(e_x(t)) \leq V(e_x(t_i)) e^{-\mu_V(t-t_i)} + c_\omega \int_{t_i}^t e_\omega(\tau)^2 e^{-\mu_V(t-\tau)} d\tau$

■ **Error bound by invoking** $\lambda_{\min}(P) \|e_x\|^2 \leq V(e_x) = e_x^\top P e_x \leq \lambda_{\max}(P) \|e_x\|^2$

$\implies \forall t \geq t_i: \|e_x(t)\|^2 \leq c_P \|e_x(t_i)\|^2 e^{-\mu_V(t-t_i)} + c'_\omega \int_{t_i}^t e_\omega(\tau)^2 e^{-\mu_V(t-\tau)} d\tau$

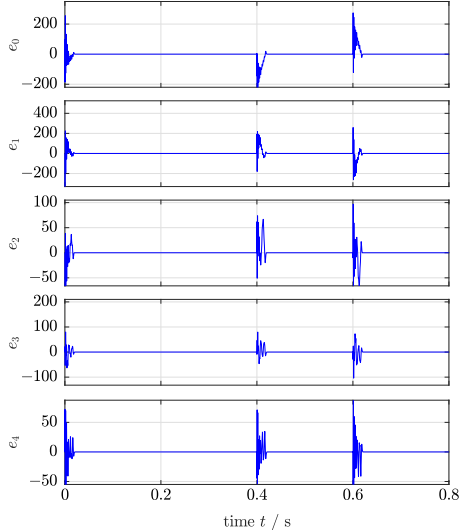
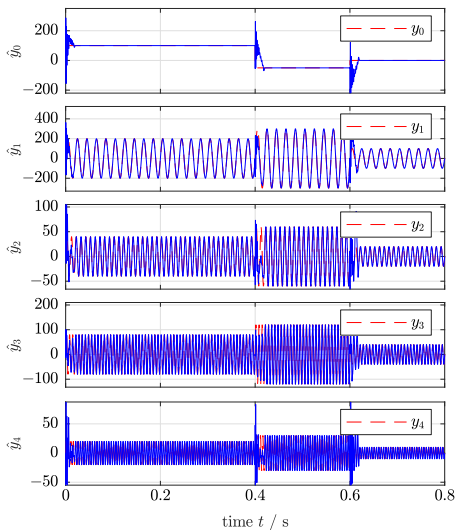
Observer design

Simulation results: Estimate $\hat{y}$, estimation error $e_y = y - \hat{y}$ and estimated frequency $\hat{f} = \frac{\hat{\omega}}{2\pi}$



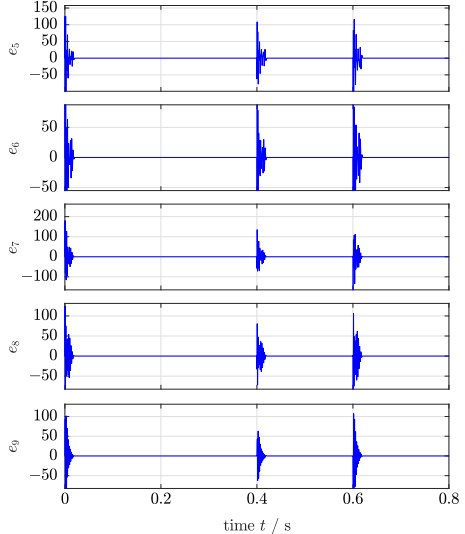
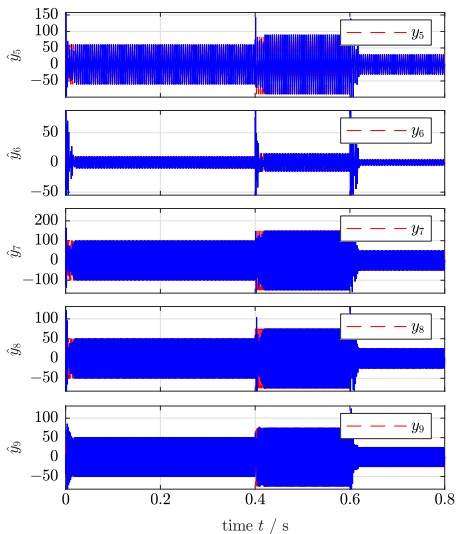
Observer design

Simulation results: Estimate $\hat{y}_\nu$ (left) and estimation error $e_\nu = y_\nu - \hat{y}_\nu$ (right)



Observer design

Simulation results: Estimate $\hat{y}_\nu$ (left) and estimation error $e_\nu = y_\nu - \hat{y}_\nu$ (right)



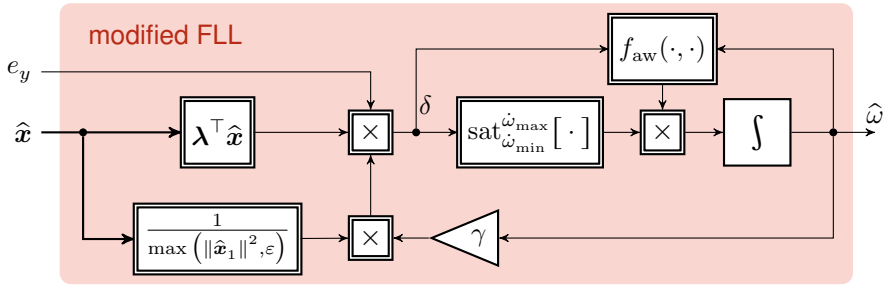
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Frequency estimation

Modified Frequency Locked Loop (mFLL) with sign-correct anti-windup and rate limitation

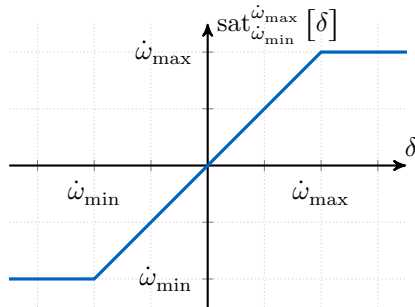


$$\frac{d}{dt}\hat{\omega} = f_{\text{aw}}(\hat{\omega}, \delta) \cdot \text{sat}_{\omega_{\min}}^{\omega_{\max}} \left[\underbrace{\frac{\gamma \hat{\omega} e_y \lambda^\top \hat{\mathbf{x}}}{\max(\|\hat{\mathbf{x}}_1\|^2, \epsilon)}}_{=:\delta} \right] = \begin{cases} > 0, & \hat{\omega} < \omega \wedge e_y \neq 0 \\ < 0, & \hat{\omega} > \omega \wedge e_y \neq 0 \end{cases}$$

$$\Leftarrow \lambda := \text{blockdiag}(0, \mathbf{J}^{-1}, \mathbf{O}_{2 \times 2}, \dots, \mathbf{O}_{2 \times 2}) \mathbf{l} \quad (\text{mFLL})$$

Frequency estimation

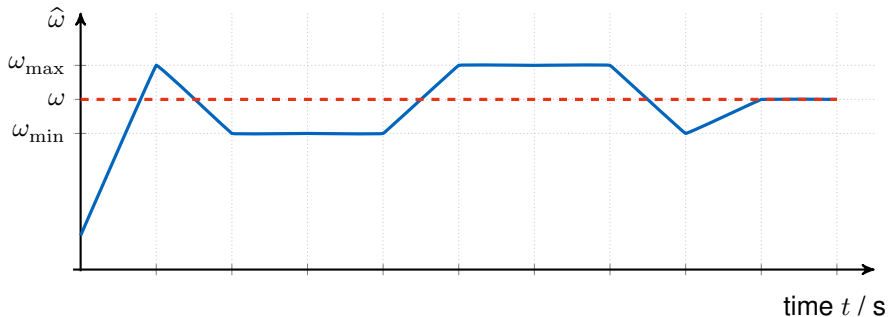
Modified FLL: Saturation of derivative of angular frequency estimate (rate limitation)



$$\text{sat}_{\dot{\omega}_{\min}}^{\dot{\omega}_{\max}}[\delta] = \begin{cases} \dot{\omega}_{\max} & , \delta > \dot{\omega}_{\max} \\ \delta & , \dot{\omega}_{\min} \leq \delta \leq \dot{\omega}_{\max} \\ \dot{\omega}_{\min} & , \delta < \dot{\omega}_{\min} \end{cases}$$

Frequency estimation

Modified FLL: Sign-correct anti-windup

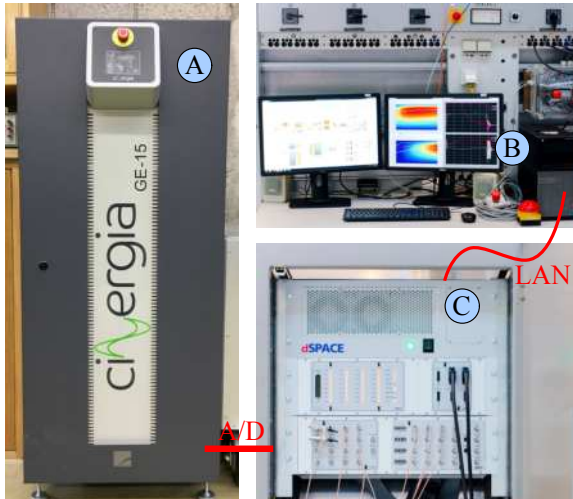


$$f_{\text{aw}}(\hat{\omega}, \frac{d}{dt}\hat{\omega}) := \begin{cases} 0, & \text{for } (\hat{\omega} \geq \omega_{\max} \wedge \frac{d}{dt}\hat{\omega} > 0) \vee (\hat{\omega} \leq \omega_{\min} \wedge \frac{d}{dt}\hat{\omega} < 0) \\ 1, & \text{else} \end{cases}$$

$$\implies \forall t \geq 0: \hat{\omega}(t) \in [\min(\omega_{\min}, \hat{\omega}_0), \min(\omega_{\max}, \hat{\omega}_0)] \implies \hat{\omega}(\cdot) \in \mathcal{L}^\infty(\mathbb{R}_{\geq 0}; \mathbb{R}_{>0})$$

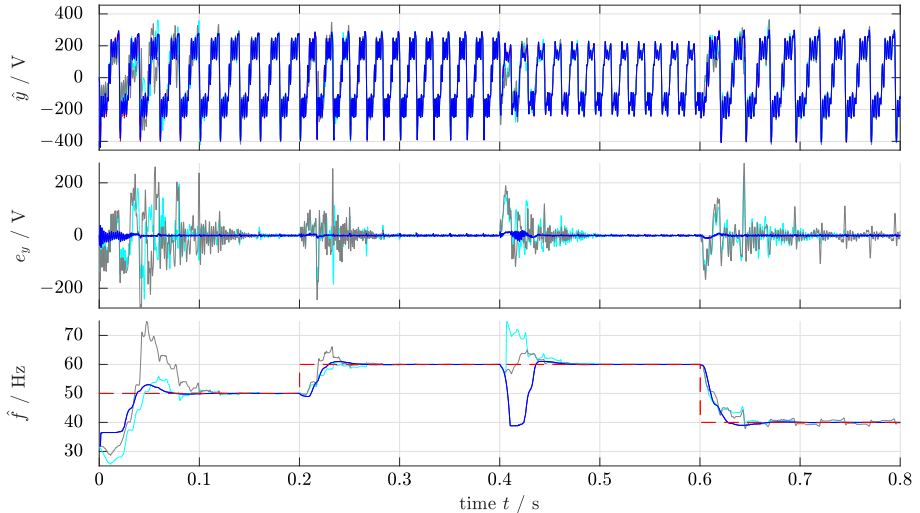
Frequency estimation

Measurement results in laboratory: (A) Grid emulator, (B) Host-PC and (C) Real-time system



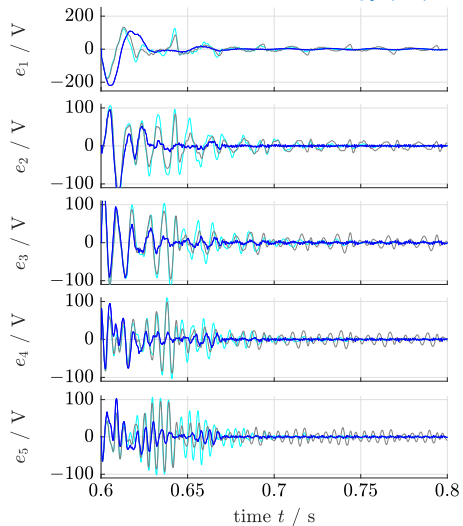
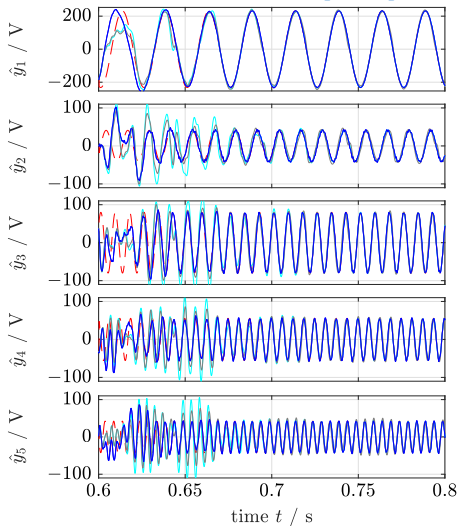
Frequency estimation

Measurement results with FLL: — mSOGI, — sSOGI, — ANF, - - - y, f



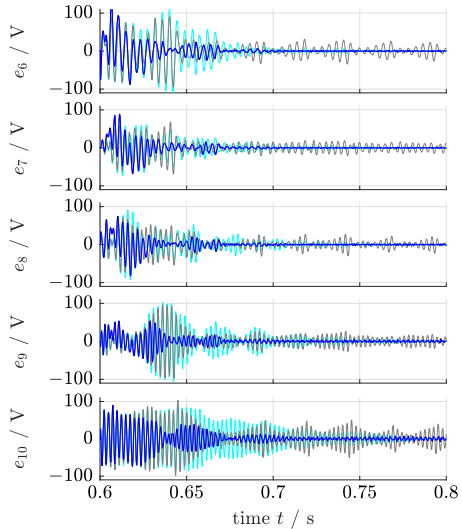
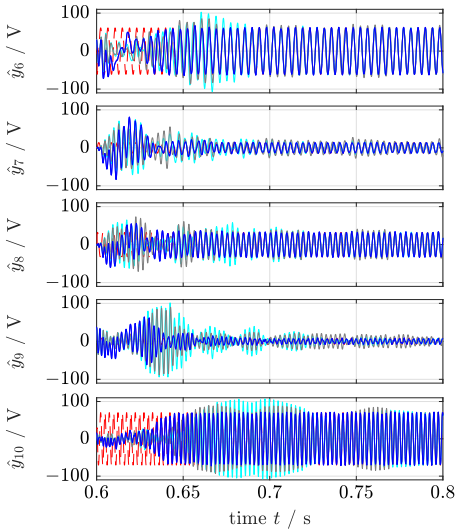
Frequency estimation

Measurement results with FLL [Zoom]: — mSOGI, — sSOGI, — ANF, - - - y_ν (left)



Frequency estimation

Measurement results with FLL [Zoom]: — mSOGI, — sSOGI, — ANF, - - - y_ν (left)



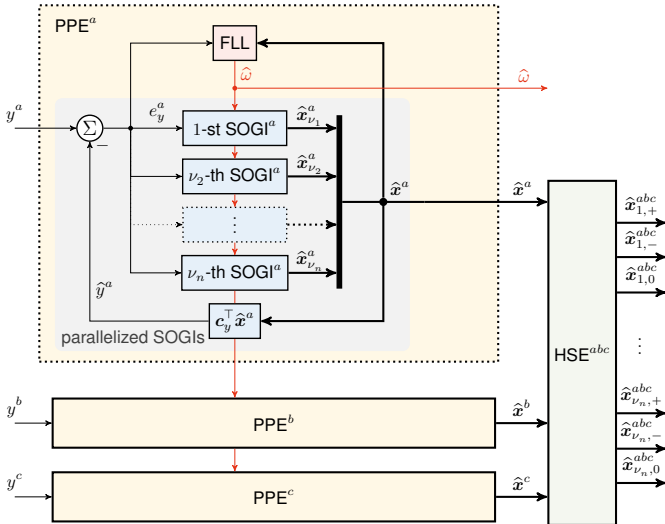
Outline I

2 Grid state estimation: An internal model based approach

- Introduction
- Internal model principle
- Observer design
- Frequency estimation
- **Harmonic sequence extraction**
- Conclusion

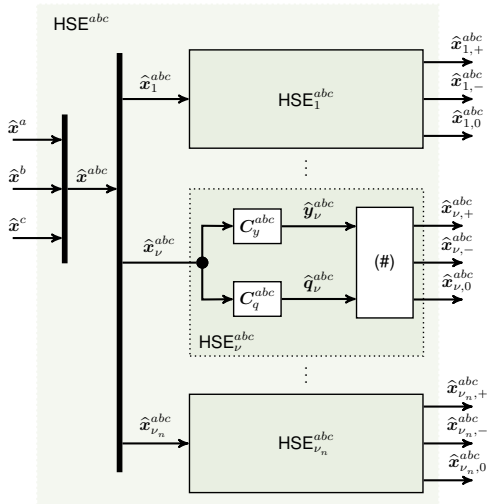
Harmonic sequence extraction

Overview: Phase parameter estimation (PPE) and Harmonic sequence extraction (HSE)



Harmonic sequence extraction

Harmonic sequence extraction (HSE) for the three phases a, b, c



Harmonic sequence extraction

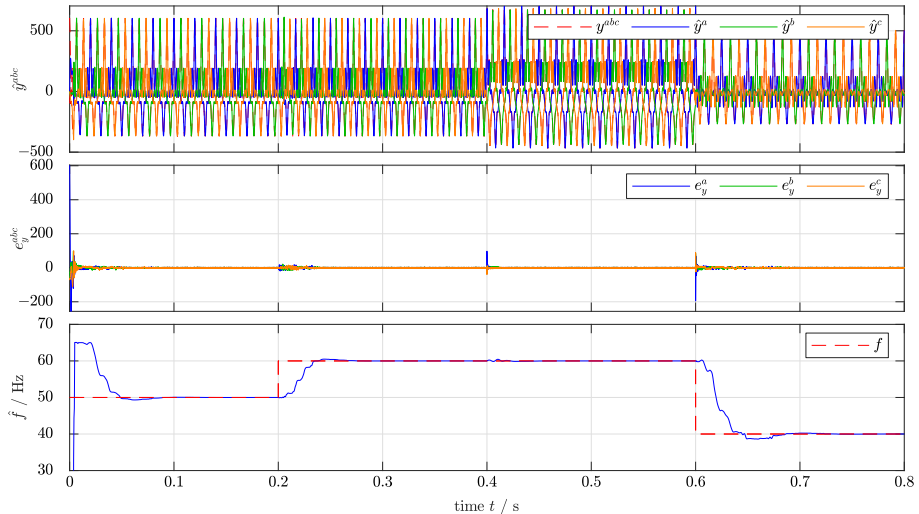
Positive, negative and zero sequence estimation of ν -th harmonic

Let $\nu \in \mathbb{H}_n$, $\mathbf{J}_1 := \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$ and $\mathbf{T}_c := \kappa \begin{bmatrix} 1 & -\frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{bmatrix}$, $\kappa \in \{\frac{2}{3}, \sqrt{\frac{2}{3}}\}$, define

$$\left. \begin{aligned}
 \mathbf{y}_\nu^{abc}(t) &= \underbrace{\frac{1}{2} \mathbf{T}_c^{-1} \overbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix}}^{=: D_{12}} \mathbf{T}_c \hat{\mathbf{y}}_\nu^{abc}(t) + \frac{1}{2} \mathbf{T}_c^{-1} \mathbf{J}_1 D_{12} \mathbf{T}_c \hat{\mathbf{q}}_\nu^{abc}(t)}_{=: \hat{\mathbf{x}}_{\nu,+}^{abc}(t) \text{ [positive sequence]}} \\
 &+ \underbrace{\frac{1}{2} \mathbf{T}_c^{-1} D_{12} \mathbf{T}_c \hat{\mathbf{y}}_\nu^{abc}(t) - \frac{1}{2} \mathbf{T}_c^{-1} \mathbf{J}_1 D_{12} \mathbf{T}_c \hat{\mathbf{q}}_\nu^{abc}(t)}_{=: \hat{\mathbf{x}}_{\nu,-}^{abc}(t) \text{ [negative sequence]}} \\
 &+ \underbrace{\mathbf{T}_c^{-1} \overbrace{\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}}^{=: D_3} \mathbf{T}_c \hat{\mathbf{y}}_\nu^{abc}(t)}_{=: \hat{\mathbf{x}}_{\nu,0}^{abc}(t) \text{ [zero sequence]}}
 \end{aligned} \right\} \quad (\#)$$

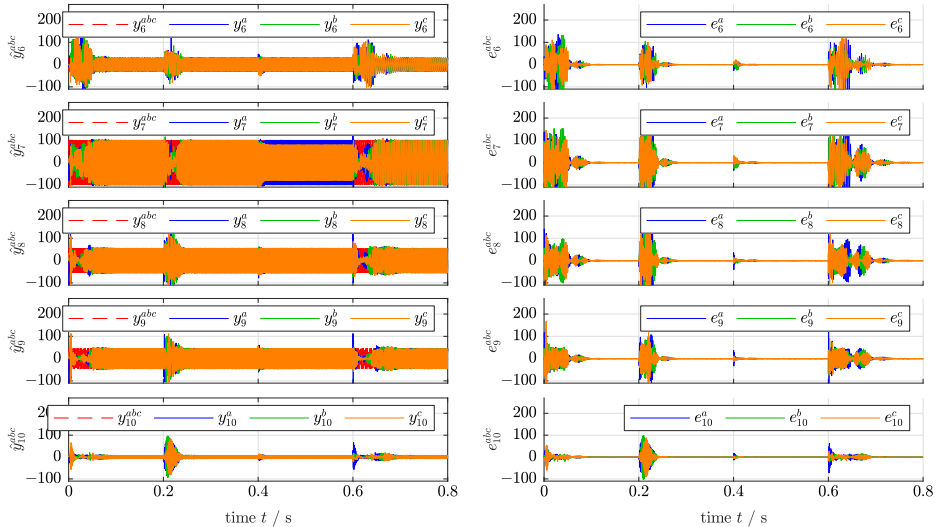
Harmonic sequence extraction

Simulation results: Estimate $\hat{y}^{abc}$, estimation error $e^{abc} = y^{abc} - \hat{y}^{abc}$ & estimated frequency $\hat{f}$



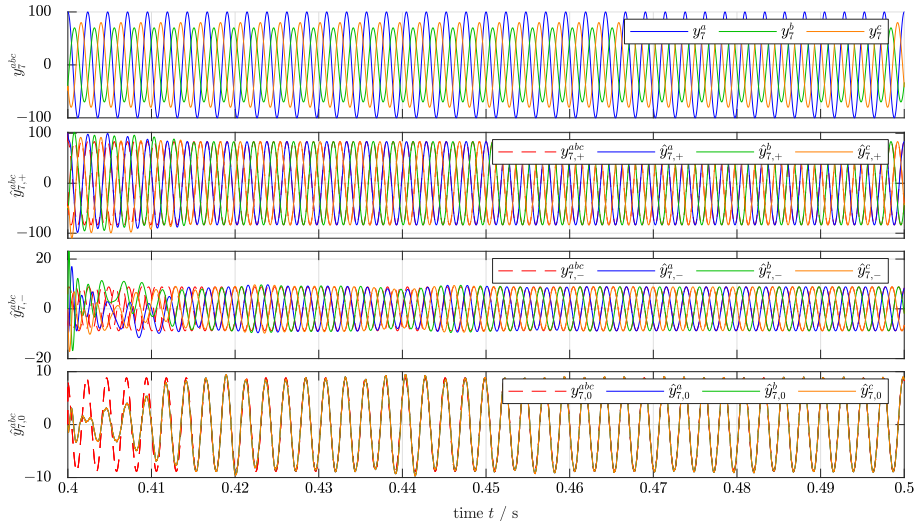
Harmonic sequence extraction

Simulation results: Estimate $\hat{y}_\nu$ (left) and estimation error $e_\nu = y_\nu - \hat{y}_\nu$ (right)



Harmonic sequence extraction

Simulation results: Harmonic y_7^{abc} , positive $\hat{y}_{7,+}^{abc}$, negative $\hat{y}_{7,-}^{abc}$ & zero $\hat{y}_{7,0}^{abc}$ sequence



Outline I

2 Grid state estimation: An internal model based approach

- Introduction
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Conclusion

Summary and outlook

To take home

- **unified theory** for grid state estimation, based on
 - **internal model principle** and **parallelization** $\implies$ observation problem;
 - **parallelized internal models** with **feedback** (mSOGIs) $\implies$ modular structure;
 - **pole placement** $\implies$ prescribed settling time
 - **modified** frequency-locked loop (FLL) with sign-correct anti-windup and rate limitation
- **real-time estimation**
- **positive, negative** and **zero sequence extraction** for each harmonic

Future work

- Frequency Locked-Loop weakest component $\implies$ further improvement
- Reduction of noise sensitivity $\implies$ (extended) Kalman filter design or pre-filtering?
- three-phase implementation, validation and test in laboratory

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