

Analytical computation of the optimal reference currents for MTPC/MTPA, MTPV and MTPF operation of anisotropic synchronous machines considering stator resistance and mutual inductance

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Motivation

Synchronous machines: Widely-used, compact and efficient actuators



www.bmw.de



www.farmwood.co.uk

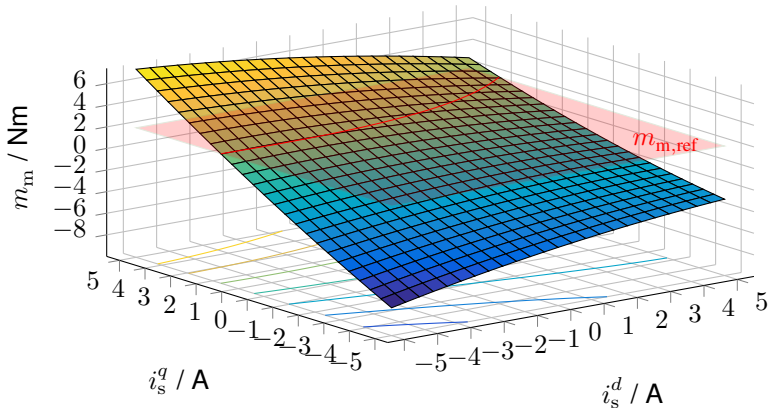


www.abb.com (from video)

- traction drives (e.g. electric vehicles or trains)
- air conditioning/fans
- pumps
- conventional power plants (e.g. hydro power plants)
- renewable energy systems (e.g. direct-drive wind turbine systems)

Motivation

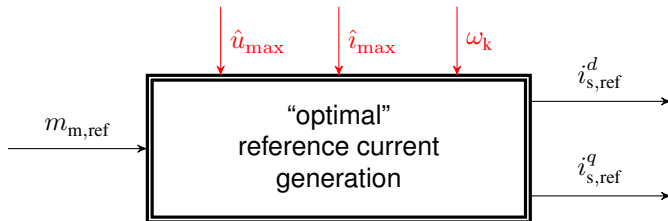
Optimal feedforward torque control problem: **Anisotropic machine**



$$m_m(i_s^d, i_s^q) = \frac{3}{2} n_p \left[\underbrace{\psi_{pm} i_s^q}_{\text{magnetic torque}} + \underbrace{(L_s^d - L_s^q) i_s^d i_s^q}_{\text{reluctance torque}} + \underbrace{L_m ((i_s^q)^2 - (i_s^d)^2)}_{\text{cross-coupling torque}} \right]$$

Motivation

Optimal feedforward torque control problem: **Goal**

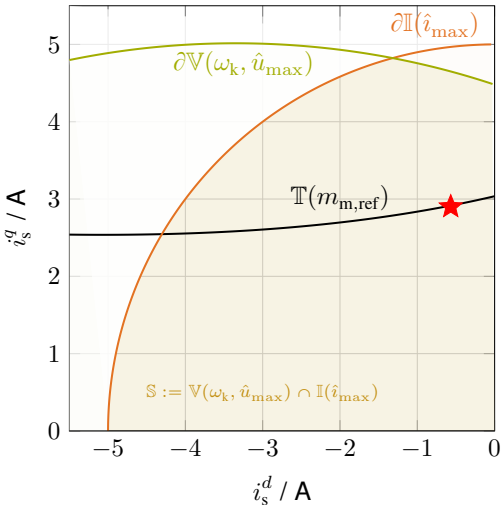


$$\mathbf{i}_{s,\text{ref}}^k(m_{m,\text{ref}}, \hat{u}_{\max}, \hat{i}_{\max}, \omega_k) = \begin{pmatrix} i_{s,\text{ref}}^d(m_{m,\text{ref}}, \hat{u}_{\max}, \hat{i}_{\max}, \omega_k) \\ i_{s,\text{ref}}^q(m_{m,\text{ref}}, \hat{u}_{\max}, \hat{i}_{\max}, \omega_k) \end{pmatrix}$$

- ✓ Numerical solutions and/or look-up tables
(but: limited storage, accuracy, real-time applicability)
- ✗ Analytical solutions (some do exist but impose simplifying assumptions such as $R_s = 0$ and/or $L_m = 0$)

Problem statement and proposed solution

Feedforward torque control: Optimization problem(s) with multiple constraints



$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} -f(\mathbf{i}_s^k) \quad \text{subject to} \\ \left\{ \begin{array}{l} \|\mathbf{i}_s^k\|^2 \leq \hat{i}_{max}^2, \\ \text{(current circular area)} \\ \|\mathbf{u}_s^k(\mathbf{i}_s^k, \omega_k)\|^2 \leq \hat{u}_{max}^2, \\ \text{(voltage elliptical area)} \\ |m_m(\mathbf{i}_s^k)| \leq |m_{m,ref}|, \text{ and} \\ \text{sign}(m_{m,ref}) = \\ \text{sign}(m_m(\mathbf{i}_s^k)). \end{array} \right. \end{aligned}$$

e.g. $-f(\mathbf{i}_s^k) = -\|\mathbf{i}_s^k\|^2$ (minimize copper losses) $\Rightarrow \mathbf{i}_{s,ref}^k$ at ★

Problem statement and proposed solution

Proposed solution: Implicit formulation (quadrics), optimization and intersection points

Step 1: Derivation of quadrics $Q_A(\mathbf{i}_s^k) := (\mathbf{i}_s^k)^\top \mathbf{A} \mathbf{i}_s^k + 2\mathbf{a}^\top \mathbf{i}_s^k + \alpha$:

- Current circular area: $(i_s^d)^2 + (i_s^q)^2 \leq \hat{i}_{\max}^2 \iff \|\mathbf{i}_s^k\|^2 = (\mathbf{i}_s^k)^\top \mathbf{I}_2 \mathbf{i}_s^k \leq \hat{i}_{\max}^2$

$$\implies \mathbb{I}(\hat{i}_{\max}) := \{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid (\mathbf{i}_s^k)^\top \mathbf{I}_2 \mathbf{i}_s^k - \hat{i}_{\max}^2 \leq 0 \}$$

- Voltage elliptical area: $(u_s^d)^2 + (u_s^q)^2 \leq \hat{u}_{\max}^2 \iff \|\mathbf{u}_s^k(\mathbf{i}_s^k, \omega_k)\|^2 = \dots \leq \hat{u}_{\max}^2$

$$\implies \mathbb{V}(\omega_k, \hat{u}_{\max}) := \{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid (\mathbf{i}_s^k)^\top \mathbf{V}(\omega_k) \mathbf{i}_s^k + 2\mathbf{v}(\omega_k)^\top \mathbf{i}_s^k + \nu(\omega_k, \hat{u}_{\max}) \leq 0 \}$$

- Reference torque hyperbola: $m_m(\mathbf{i}_s^k) = \frac{3}{2} n_p (\mathbf{i}_s^k)^\top \mathbf{J} \boldsymbol{\psi}_s^k(\mathbf{i}_s^k) \stackrel{!}{=} m_{m,\text{ref}} \iff \dots$

$$\implies \mathbb{T}(m_{m,\text{ref}}) := \{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid (\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2\mathbf{t}^\top \mathbf{i}_s^k - m_{m,\text{ref}} = 0 \}$$

- ...

Problem statement and proposed solution

Proposed solution: Implicit formulation (quadrics), optimization and intersection points (cont'd)

Step 2: Optimization problem with equality constraint

$$\max_{\mathbf{i}_s^k} - \left(\underbrace{(\mathbf{i}_s^k)^\top \mathbf{A} \mathbf{i}_s^k + 2\mathbf{a}^\top \mathbf{i}_s^k + \alpha}_{=: Q_A(\mathbf{i}_s^k)} \right) \text{ s.t. } \underbrace{(\mathbf{i}_s^k)^\top \mathbf{B} \mathbf{i}_s^k + 2\mathbf{b}^\top \mathbf{i}_s^k + \beta}_{=: Q_B(\mathbf{i}_s^k)} = 0$$

$\implies$ Hyperbolas for MTPC, MTPV and MTPF (with $R_s \neq 0$ & $L_m \neq 0$!)

Step 3: Intersection of two quadrics (e.g. voltage ellipse and current circle)

$$\mathbf{i}_{s,\text{ref}}^k := \arg \min_{\|\mathbf{i}_s^k\|} \left\{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid Q_A(\mathbf{i}_s^k) = 0 \wedge Q_B(\mathbf{i}_s^k) = 0 \right\}$$

$\implies$ Optimal operation point ★ (reference current)

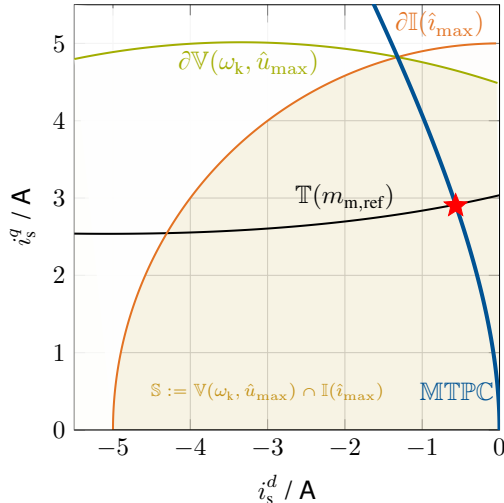
Both lead to subproblem of solving a fourth-order (quartic) polynomial

$$\chi(\lambda) := c_4 \lambda^4 + c_3 \lambda^3 + c_2 \lambda^2 + c_1 \lambda + c_0 \stackrel{!}{=} 0$$

$\implies$ Analytical solutions exist (e.g. Euler's solution, see [1])

Operation management and operation strategies

Maximum Torque per Current (**MTPC**): Reference torque feasible



Optimization problem

$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} \quad & -\|\mathbf{i}_s^k\|^2 \quad \text{s.t.} \\ & \underbrace{(\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2 \mathbf{t}^\top \mathbf{i}_s^k}_{=m_m(\mathbf{i}_s^k)} - m_{m,ref} = 0 \end{aligned}$$

Solution set

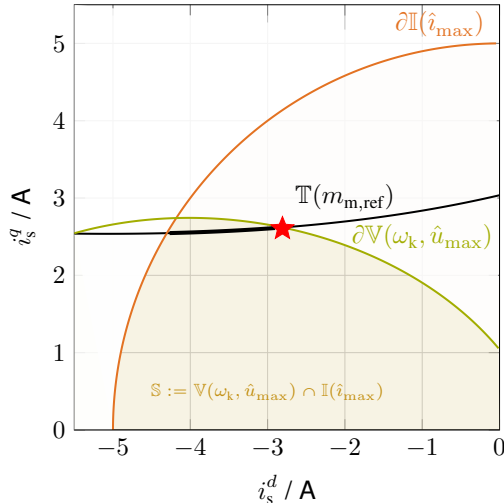
$$\begin{aligned} \text{MTPC} := \{ & \mathbf{i}_s^k \in \mathbb{R}^2 \mid \\ & (\mathbf{i}_s^k)^\top \mathbf{M}_C \mathbf{i}_s^k + 2 \mathbf{m}_C^\top \mathbf{i}_s^k = 0 \} \end{aligned}$$

Optimal current reference (★)

$$\mathbf{i}_{s,ref}^k = \text{MTPC} \cap T(m_{m,ref})$$

Operation management and operation strategies

Field Weakening (FW): Reference torque feasible



Optimization problem

$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} & -\|\mathbf{i}_s^k\|^2 \quad \text{s.t.} \\ & \underbrace{(\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2 \mathbf{t}^\top \mathbf{i}_s^k}_{=m_m(\mathbf{i}_s^k)} - m_{m,\text{ref}} = 0 \end{aligned}$$

Feasible set

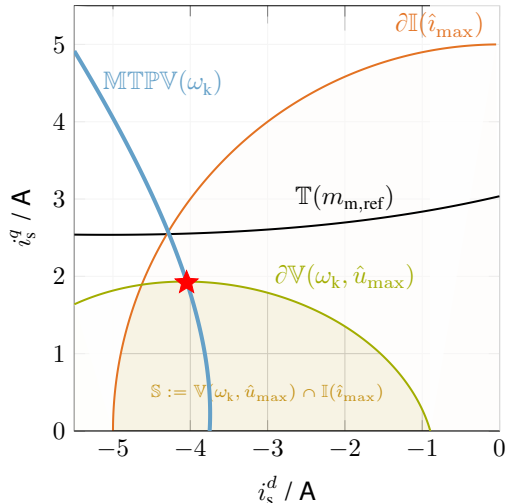
$$\begin{aligned} \text{FW}(m_{m,\text{ref}}, \omega_k, \hat{u}_{\max}) &:= \\ & \mathbb{S}(\omega_k, \hat{u}_{\max}, \hat{i}_{\max}) \cap \mathbb{T}(m_{m,\text{ref}}) \end{aligned}$$

Optimal current reference (★)

$$\mathbf{i}_{s,\text{ref}}^k = \partial \mathbb{V}(\omega_k, \hat{u}_{\max}) \cap \mathbb{T}(m_{m,\text{ref}})$$

Operation management and operation strategies

Maximum Torque per Voltage (**MTPV**): Reference torque **not** feasible



Optimization problem

$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} \quad & -\|\mathbf{u}_s^k(\mathbf{i}_s^k)\|^2 \quad \text{s.t.} \\ & \underbrace{(\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2 \mathbf{t}^\top \mathbf{i}_s^k}_{=m_m(\mathbf{i}_s^k)} - m_{m,\text{ref}} = 0 \end{aligned}$$

Solution set

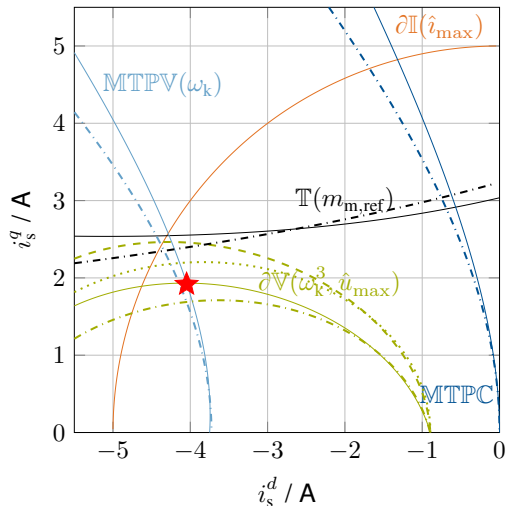
$$\begin{aligned} \text{MTPV}(\omega_k) := \{ & \mathbf{i}_s^k \in \mathbb{R}^2 \mid \\ & (\mathbf{i}_s^k)^\top \mathbf{M}_V \mathbf{i}_s^k + 2 \mathbf{m}_V^\top \mathbf{i}_s^k + \mu_V = 0 \} \end{aligned}$$

Optimal current reference (★)

$$\mathbf{i}_{s,\text{ref}}^k = \text{MTPV}(\omega_k) \cap \partial \mathcal{V}(\omega_k, \hat{u}_{\max})$$

Operation management and operation strategies

Illustration of the effect of neglecting R_s and/or L_m



--- $R_s = 0$ (and $L_m \neq 0$)

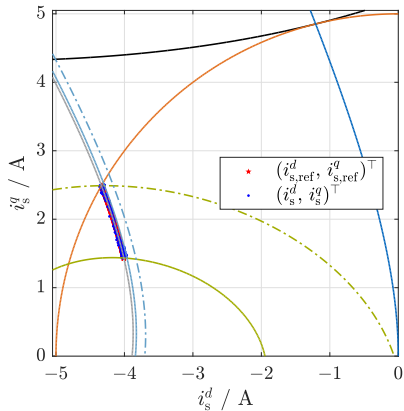
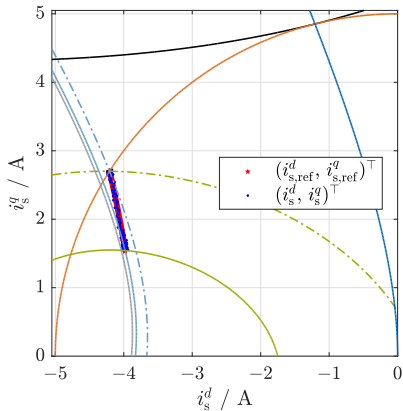
- - - $L_m = 0$ (and $R_s \neq 0$)

..... $R_s = 0$ and $L_m = 0$

⇒ **Reduced efficiency!**
(and wrong torque and/or possibly wrong operation strategies)

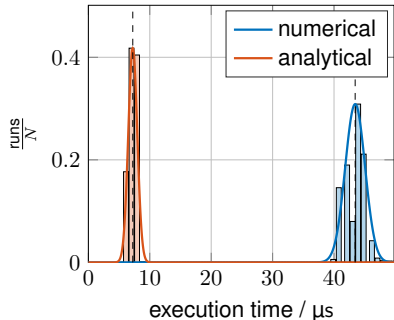
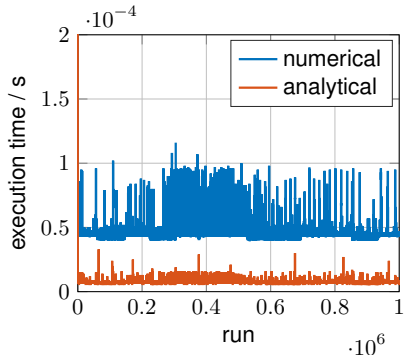
Implementation results

Simulation (including switching behavior): MTPV and MTPF



Implementation results

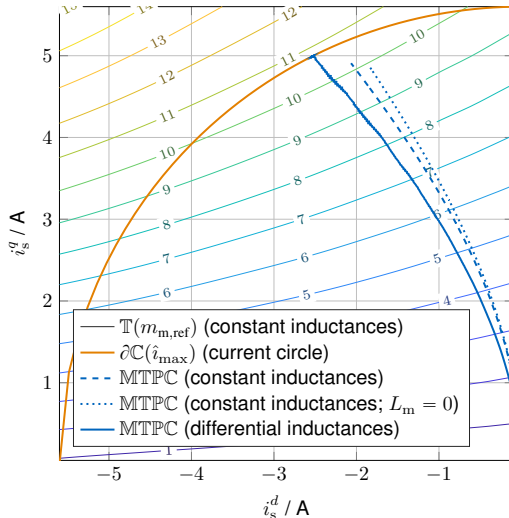
Experiments: Comparison of the computational load (Euler's solution for fourth-order polynomials)



- Execution times for $N = 10^6$ runs (downsampled by factor 100);
- Average execution times $\mu_n = 43,4 \cdot 10^{-6}$ s and $\mu_a = 7,23 \cdot 10^{-6}$ s; and
- Standard deviations $\sigma_n = 1,61 \cdot 10^{-6}$ s and $\sigma_a = 0,73 \cdot 10^{-6}$ s.

Implementation results

Experiments: MTPC at a IPMSM with non-negligible mutual inductance and nonlinear flux linkage



Conclusion

Summary and future work

To take home

- **unified** theory for MTPC, FW, MTPV/MTPF or MC based on
 - **quadrics** (implicit formulation),
 - **optimization problems** with **equality constraint**, and
 - **intersection** of two quadrics
- **analytical** solution for reference currents (& transition points)
- $R_s \neq 0$ and $L_m \neq 0$ (both can be considered **simultaneously**)
- **fast(er)** and **more accurate** computation
- **applicable** in real-world (nonlinear RSM and IPMSM)

Future work

- convergence (mathematical proof or consideration of nonlinear flux linkages)
- consideration of iron losses (including e.g. $R_{fe}(\omega_k)$; article in preparation)
- impact of parameter uncertainty (e.g. $R_s^a \neq R_s^b \neq R_s^c$; article in preparation)

References I

- [1] R.W.D Nickalls. The quartic equation: Invariants and Euler's solution revealed. *Mathematical Gazette*, 93(526):66–75, 2009.