

Optimal feedforward torque control of anisotropic synchronous machines with analytical solution considering stator resistance and cross-coupling inductance

Christoph Hackl

IEEE Senior Member

Technische Universität München (TUM)

Munich School of Engineering (MSE)

MSE Research group "Control of Renewable Energy Systems (CRES)"

www.cres.mse.tum.de

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Technische Universität Kaiserslautern

Outline

- 1 Scientific background
- 2 Optimal feedforward torque control of anisotropic synchronous machines with analytical solution [1–4]

Outline

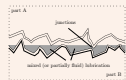
- 1 Scientific background
 - Interdisciplinary expertise
 - Research group “Control of renewable energy systems (CRES)”
 - Running projects and third-party funding
 - Teaching experience

Scientific background

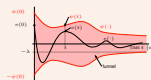
Interdisciplinary expertise (> 90 peer-reviewed publications, e.g. one monograph)



System identification
[13–17]



Dynamic friction
[18, 19]



Non-identifier based adaptive control [18, 20–35]



Paper coating machines
[8–12]



Teaching
(EOF Award '13)
[35, 95–101]



Robotics / mechatronics
[18, 19, 35–46]



Electro-active polymers
[5–7]

Systems & control
(dynamical systems)



Power electronics
[35, 35, 47–66]



Renewable energy systems
[17, 32, 34, 35, 48, 49, 52, 56, 57, 59–61, 63, 65, 66, 71–73, 76, 78, 84–94]



Electrical drives (machines/generators)
[17, 18, 20, 22, 23, 33, 35, 41, 45, 58, 67–84]

Scientific background

Head of CRES research group (since 2014): 9 PhD students, 1 Post-Doc (& 3 PhD collaborations)

Team



H. Eldeeb, M.Sc.
(CRES, 09/2015)



C. Dirscherl, M.Sc.
(CRES, 01/2014)



C. Hackl, Dr.-Ing.
(CRES, 01/2014)



J. Kullick, M.Sc.
(CRES, 10/2015)



K. Schechner, M.Sc.
(CRES, 01/2014)



C. Ladisla, M.Sc.
(CRES, 01/2018)

External PhD students



M. Landerer, M.Sc.
(CRES, 06/2016)



Z. Zhang, Dr.-Ing.
(CRES/EAL, 07/2015)



K. Bär, M.Sc.
(THI, 07/2017)



A. Birda, M.Sc.
(BMW, 04/2016)



S. Krüner, M.Sc.
(SINNPower, 11/2015)

Scientific background

Running projects & third-party funding (> 2 million €; e.g. DAAD, Bavaria, BMBF, BMWi, DFG, EU)

Large-scale WTS



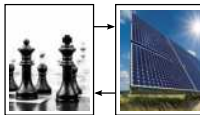
Efficiency+Reliability

Small-scale WTS



Reluctance SM

Model predictive control for RES



Real-time applicability

Airborne Wind Energy



Fault-tolerant control

Geothermal energy



Fault-tolerant control

Wave energy (SinnPower)



Efficiency+Reliability

Electric vehicles (BMW)



Efficiency+Reliability

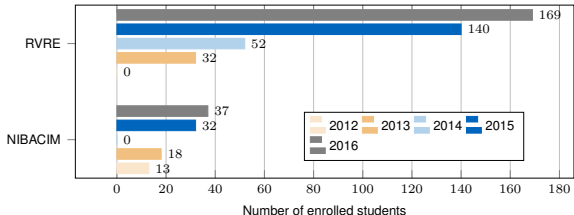
Electrical power system



Three-phase four-wire system dynamics

Scientific background

Teaching experience (since 2004)



- Lectures, tutorials, practical courses & student projects, e.g.
 - “**R**egelung von regenerativen **E**nergiesystemen” (WS, 3SWS; since 2013)
 - “**N**on-identifier based adaptive control in **m**echatronics” (SS, 4SWS; since 2012)
 - “Projektstudium Antriebstechnik” [99–101] (EOF Lehrpreis 2013, WS1415)
- International / PhD teaching activities
 - Lecture & Seminar on “Modeling and control of renewable energy systems” (TUM-CREATE, Singapore; May-July 2017)
 - EU H2020 ITN Workshop “Electrical Drives and Predictive Control” (2016)
 - MSE Winter School “Holistic Modeling and Control of Energy Systems” (2015)
 - Block course on “Modeling and control of wind turbine systems: An introduction” (South Africa, University of Stellenbosch, 2014)

Outline

2 Optimal feedforward torque control of anisotropic synchronous machines with analytical solution [1–4]

- Motivation
- Problem statement and proposed solution
- Operation management and operation strategies
- Analytical solution
- Implementation
- Conclusion

Motivation

Synchronous machines: Widely-used, compact and efficient actuators



www.bmw.de



www.farmwood.co.uk

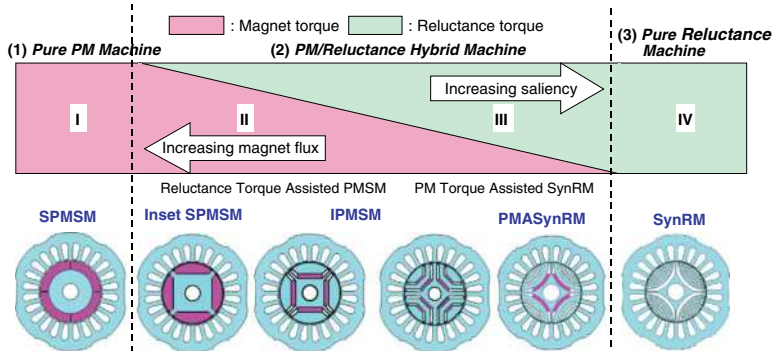


www.abb.com (from video)

- traction drives (e.g. electric vehicles or trains)
- air conditioning/fans
- pumps
- conventional power plants (e.g. hydro power plants)
- renewable energy systems (e.g. direct-drive wind turbine systems)

Motivation

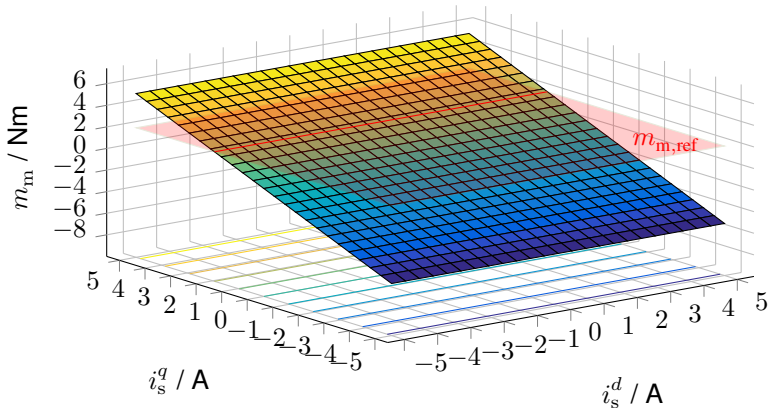
Examples of anisotropic synchronous machines [102] with “saliency ratio” $L_s^d/L_s^q \neq 1$



$$m_m(i_s^d, i_s^q) = \frac{3}{2} n_p \left[\underbrace{\psi_{pm} i_s^q}_{\text{magnetic torque}} + \underbrace{(L_s^d - L_s^q) i_s^d i_s^q}_{\text{reluctance torque}} + \underbrace{L_m ((i_s^q)^2 - (i_s^d)^2)}_{\text{cross-coupling torque}} \right]$$

Motivation

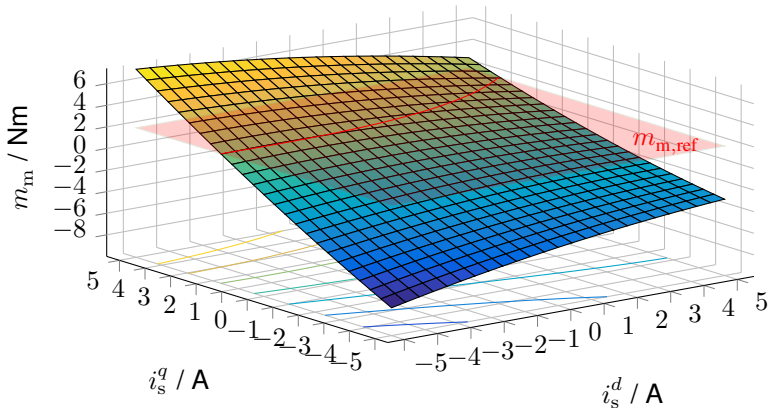
Optimal feedforward torque control problem: **Isotropic machine**



$$m_{m,ref} \stackrel{!}{=} m_m(i_s^d, i_s^q) = \frac{3}{2} n_p \psi_{pm} i_s^q \quad (\implies i_{s,ref}^q = \frac{2 m_{m,ref}}{3 n_p \psi_{pm}})$$

Motivation

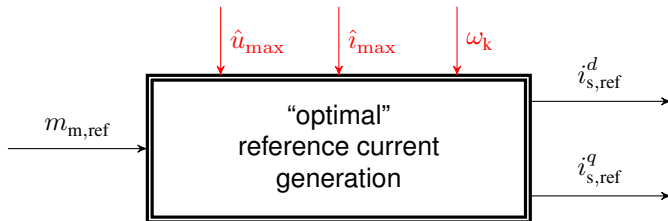
Optimal feedforward torque control problem: **Anisotropic machine**



$$m_{m,ref} \stackrel{!}{=} m_m(i_s^d, i_s^q) = \frac{3}{2} n_p \left[\psi_{pm} i_s^q + (L_s^d - L_s^q) i_s^d i_s^q + L_m ((i_s^q)^2 - (i_s^d)^2) \right]$$

Motivation

Optimal feedforward torque control problem: **Goal**



$$\mathbf{i}_{s,\text{ref}}^k(m_{m,\text{ref}}, \hat{u}_{\max}, \hat{i}_{\max}, \omega_k) = \begin{pmatrix} i_{s,\text{ref}}^d(m_{m,\text{ref}}, \hat{u}_{\max}, \hat{i}_{\max}, \omega_k) \\ i_{s,\text{ref}}^q(m_{m,\text{ref}}, \hat{u}_{\max}, \hat{i}_{\max}, \omega_k) \end{pmatrix}$$

- ✓ Numerical solutions and/or look-up tables
(but: limited storage, accuracy, real-time applicability)
- ? Analytical solutions (some do exist but impose simplifying assumptions
such as ~~$R_s = 0$ and/or $L_m = 0$~~)

Problem statement and proposed solution

Considered machines: Anisotropic synchronous machines (steady-state model)

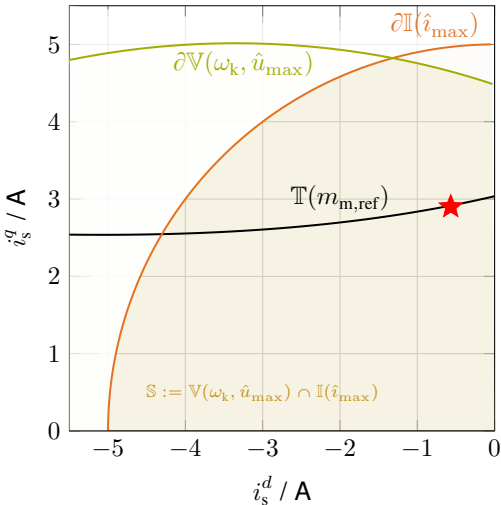
$$\begin{aligned}
 \underbrace{\begin{pmatrix} u_s^d(\mathbf{i}_s^k, \omega_k) \\ u_s^q(\mathbf{i}_s^k, \omega_k) \end{pmatrix}}_{=: \mathbf{u}_s^k(\mathbf{i}_s^k, \omega_k)} &= R_s \underbrace{\begin{pmatrix} i_s^d \\ i_s^q \end{pmatrix}}_{=: \mathbf{i}_s^k} + \omega_k \underbrace{\begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}}_{=: \mathbf{J}} \underbrace{\begin{pmatrix} \psi_s^d(\mathbf{i}_s^k) \\ \psi_s^q(\mathbf{i}_s^k) \end{pmatrix}}_{=: \boldsymbol{\psi}_s^k(\mathbf{i}_s^k)} + \cancel{\frac{d}{dt} \boldsymbol{\psi}_s^k(\mathbf{i}_s^k)} \\
 m_m(\mathbf{i}_s^k) &= \frac{3}{2} n_p (\mathbf{i}_s^k)^\top \mathbf{J} \boldsymbol{\psi}_s^k(\mathbf{i}_s^k) \\
 &= \frac{3}{2} n_p \left[\psi_{pm} i_s^q + (L_s^d - L_s^q) i_s^d i_s^q + L_m ((i_s^q)^2 - (i_s^d)^2) \right]
 \end{aligned}$$

Assumption (Affine flux linkage (at least locally))

$$\boldsymbol{\psi}_s^k(\mathbf{i}_s^k) = \underbrace{\begin{bmatrix} L_s^d & L_m \\ L_m & L_s^q \end{bmatrix}}_{=: \mathbf{L}_s^k \in \mathbb{R}^{2 \times 2}} \mathbf{i}_s^k + \underbrace{\begin{pmatrix} \psi_{pm} \\ 0 \end{pmatrix}}_{=: \boldsymbol{\psi}_{pm}^k} \quad \text{with } \mathbf{L}_s^k = (\mathbf{L}_s^k)^\top > 0$$

Problem statement and proposed solution

Feedforward torque control: Optimization problem(s) with multiple constraints



$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} -f(\mathbf{i}_s^k) \quad \text{subject to} \\ \left\{ \begin{array}{l} \|\mathbf{i}_s^k\|^2 \leq \hat{i}_{max}^2, \\ \text{(current circular area)} \\ \|\mathbf{u}_s^k(\mathbf{i}_s^k, \omega_k)\|^2 \leq \hat{u}_{max}^2, \\ \text{(voltage elliptical area)} \\ |m_m(\mathbf{i}_s^k)| \leq |m_{m,ref}|, \text{ and} \\ \text{sign}(m_{m,ref}) = \\ \text{sign}(m_m(\mathbf{i}_s^k)). \end{array} \right. \end{aligned}$$

e.g. $-f(\mathbf{i}_s^k) = -\|\mathbf{i}_s^k\|^2$ (minimize copper losses) $\Rightarrow \mathbf{i}_{s,ref}^k$ at ★

Problem statement and proposed solution

Proposed solution: Implicit formulation (quadrics), optimization and intersection points

Step 1: Derivation of quadrics $Q_A(\mathbf{i}_s^k) := (\mathbf{i}_s^k)^\top \mathbf{A} \mathbf{i}_s^k + 2\mathbf{a}^\top \mathbf{i}_s^k + \alpha$:

- Current circular area: $(i_s^d)^2 + (i_s^q)^2 \leq \hat{i}_{\max}^2 \iff \|\mathbf{i}_s^k\|^2 = (\mathbf{i}_s^k)^\top \mathbf{I}_2 \mathbf{i}_s^k \leq \hat{i}_{\max}^2$

$$\implies \mathbb{I}(\hat{i}_{\max}) := \{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid (\mathbf{i}_s^k)^\top \mathbf{I}_2 \mathbf{i}_s^k - \hat{i}_{\max}^2 \leq 0 \}$$

- Voltage elliptical area: $(u_s^d)^2 + (u_s^q)^2 \leq \hat{u}_{\max}^2 \iff \|\mathbf{u}_s^k(\mathbf{i}_s^k, \omega_k)\|^2 = \dots \leq \hat{u}_{\max}^2$

$$\implies \mathbb{V}(\omega_k, \hat{u}_{\max}) := \{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid (\mathbf{i}_s^k)^\top \mathbf{V}(\omega_k) \mathbf{i}_s^k + 2\mathbf{v}(\omega_k)^\top \mathbf{i}_s^k + \nu(\omega_k, \hat{u}_{\max}) \leq 0 \}$$

- Reference torque hyperbola: $m_m(\mathbf{i}_s^k) = \frac{3}{2} n_p (\mathbf{i}_s^k)^\top \mathbf{J} \boldsymbol{\psi}_s^k(\mathbf{i}_s^k) \stackrel{!}{=} m_{m,\text{ref}} \iff \dots$

$$\implies \mathbb{T}(m_{m,\text{ref}}) := \{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid (\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2\mathbf{t}^\top \mathbf{i}_s^k - m_{m,\text{ref}} = 0 \}$$

- ...

Problem statement and proposed solution

Proposed solution: Implicit formulation (quadrics), optimization and intersection points (cont'd)

Step 2: Optimization problem with equality constraint

$$\max_{\mathbf{i}_s^k} - \left(\underbrace{(\mathbf{i}_s^k)^\top \mathbf{A} \mathbf{i}_s^k + 2\mathbf{a}^\top \mathbf{i}_s^k + \alpha}_{=: Q_A(\mathbf{i}_s^k)} \right) \text{ s.t. } \underbrace{(\mathbf{i}_s^k)^\top \mathbf{B} \mathbf{i}_s^k + 2\mathbf{b}^\top \mathbf{i}_s^k + \beta}_{=: Q_B(\mathbf{i}_s^k)} = 0$$

$\implies$ Hyperbolas for MTPC, MTPV and MTPF (with $R_s \neq 0$ & $L_m \neq 0$!)

Step 3: Intersection of two quadrics (e.g. voltage ellipse and current circle)

$$\mathbf{i}_{s,\text{ref}}^k := \arg \min_{\|\mathbf{i}_s^k\|} \left\{ \mathbf{i}_s^k \in \mathbb{R}^2 \mid Q_A(\mathbf{i}_s^k) = 0 \wedge Q_B(\mathbf{i}_s^k) = 0 \right\}$$

$\implies$ Optimal operation point ★ (reference current)

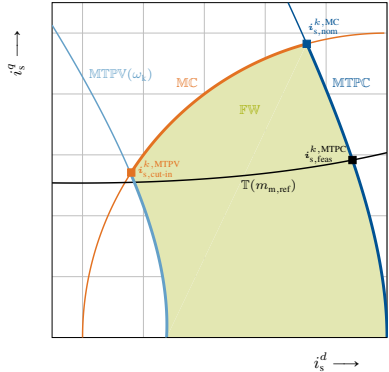
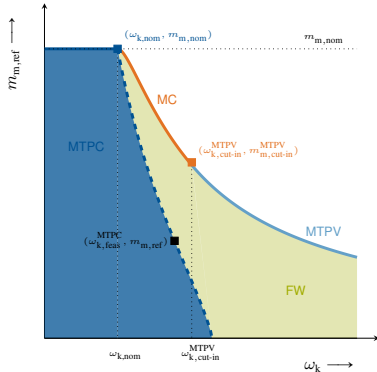
Both lead to subproblem of solving a fourth-order (quartic) polynomial

$$\chi(\lambda) := c_4 \lambda^4 + c_3 \lambda^3 + c_2 \lambda^2 + c_1 \lambda + c_0 \stackrel{!}{=} 0$$

$\implies$ Analytical solutions exist (e.g. Euler's solution, see [103])

Operation management and operation strategies

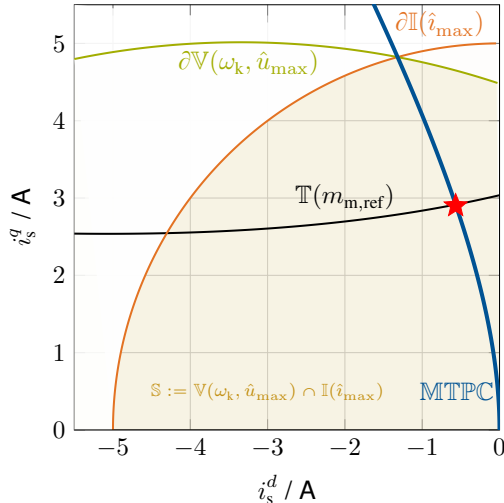
Operation management: Operation strategies and transition points



- **Maximum Torque per Current (MTPC):** $\omega_k \leq \omega_{k,\text{feas}}^{\text{MTPC}}(m_{m,\text{ref}})$ (and $m_{m,\text{ref}} \leq m_{m,\text{nom}}$)
- **Field Weakening (FW):** $\omega_{k,\text{feas}}^{\text{MTPC}}(m_{m,\text{ref}}) < \omega_k$ and $m_{m,\text{ref}} < m_{m,\text{feas}}^{\text{FW}}(\omega_k)$
- **Maximum Current (MC):** $\omega_{k,\text{nom}} < \omega_k < \omega_{k,\text{cut-in}}^{\text{MTPV}}$ and $m_{m,\text{ref}} \geq m_{m,\text{feas}}^{\text{FW}}(\omega_k)$
- **Maximum Torque per Voltage (MTPV):** $\omega_k > \omega_{k,\text{cut-in}}^{\text{MTPV}}$ and $m_{m,\text{ref}} \geq m_{m,\text{cut-in}}^{\text{MTPV}}(\omega_k)$

Operation management and operation strategies

Maximum Torque per Current (**MTPC**): Reference torque feasible



Optimization problem

$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} \quad & -\|\mathbf{i}_s^k\|^2 \quad \text{s.t.} \\ & \underbrace{(\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2 \mathbf{t}^\top \mathbf{i}_s^k}_{=m_m(\mathbf{i}_s^k)} - m_{m,ref} = 0 \end{aligned}$$

Solution set

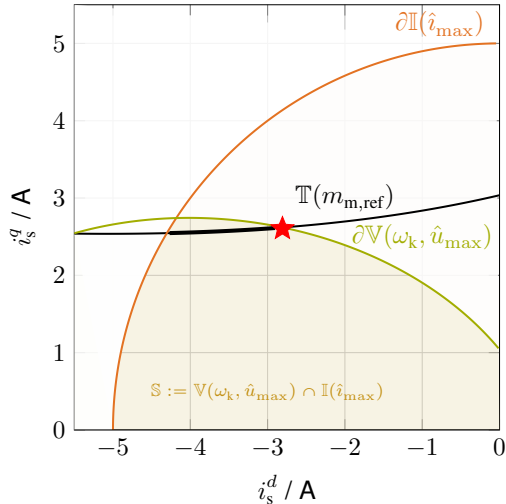
$$\begin{aligned} \text{MTPC} := \{ & \mathbf{i}_s^k \in \mathbb{R}^2 \mid \\ & (\mathbf{i}_s^k)^\top \mathbf{M}_C \mathbf{i}_s^k + 2 \mathbf{m}_C^\top \mathbf{i}_s^k = 0 \} \end{aligned}$$

Optimal current reference (★)

$$\mathbf{i}_{s,ref}^k = \text{MTPC} \cap T(m_{m,ref})$$

Operation management and operation strategies

Field Weakening (FW): Reference torque feasible



Optimization problem

$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} & -\|\mathbf{i}_s^k\|^2 \quad \text{s.t.} \\ & \underbrace{(\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2 \mathbf{t}^\top \mathbf{i}_s^k}_{=m_m(\mathbf{i}_s^k)} - m_{m,\text{ref}} = 0 \end{aligned}$$

Feasible set

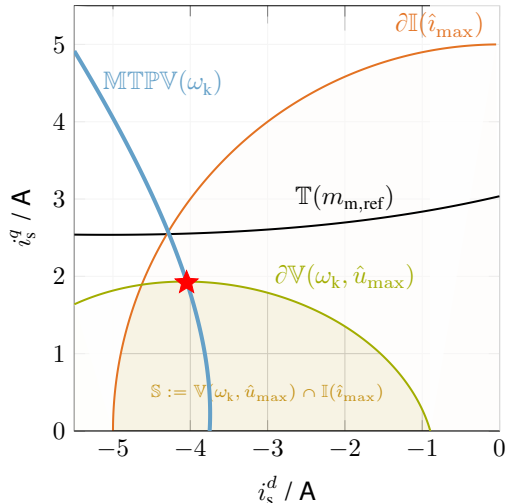
$$\begin{aligned} \text{FW}(m_{m,\text{ref}}, \omega_k, \hat{u}_{\max}) &:= \\ & \mathbb{S}(\omega_k, \hat{u}_{\max}, \hat{i}_{\max}) \cap \mathbb{T}(m_{m,\text{ref}}) \end{aligned}$$

Optimal current reference (★)

$$\mathbf{i}_{s,\text{ref}}^k = \partial \mathbb{V}(\omega_k, \hat{u}_{\max}) \cap \mathbb{T}(m_{m,\text{ref}})$$

Operation management and operation strategies

Maximum Torque per Voltage (**MTPV**): Reference torque **not** feasible



Optimization problem

$$\begin{aligned} \max_{\mathbf{i}_s^k \in \mathbb{S}} \quad & -\|\mathbf{u}_s^k(\mathbf{i}_s^k)\|^2 \quad \text{s.t.} \\ & \underbrace{(\mathbf{i}_s^k)^\top \mathbf{T} \mathbf{i}_s^k + 2 \mathbf{t}^\top \mathbf{i}_s^k}_{=m_m(\mathbf{i}_s^k)} - m_{m,\text{ref}} = 0 \end{aligned}$$

Solution set

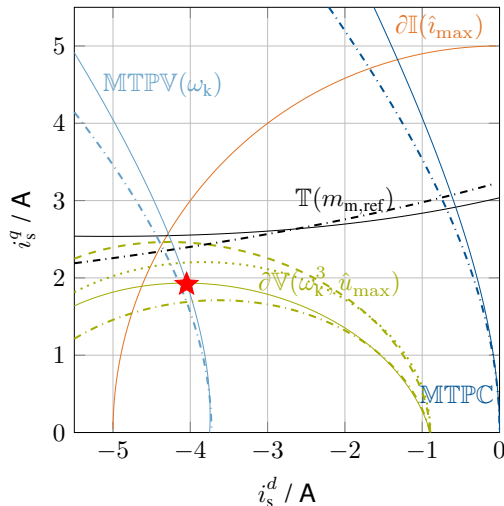
$$\begin{aligned} \text{MTPV}(\omega_k) := \{ & \mathbf{i}_s^k \in \mathbb{R}^2 \mid \\ & (\mathbf{i}_s^k)^\top \mathbf{M}_V \mathbf{i}_s^k + 2 \mathbf{m}_V^\top \mathbf{i}_s^k + \mu_V = 0 \} \end{aligned}$$

Optimal current reference (★)

$$\mathbf{i}_{s,\text{ref}}^k = \text{MTPV}(\omega_k) \cap \partial \mathcal{V}(\omega_k, \hat{u}_{\max})$$

Operation management and operation strategies

Illustration of the effect of neglecting R_s and/or L_m



--- $R_s = 0$ (and $L_m \neq 0$)

-.-.- $L_m = 0$ (and $R_s \neq 0$)

..... $R_s = 0$ and $L_m = 0$

$\Rightarrow$ **Reduced efficiency!**
(and wrong torque and/or possibly wrong operation strategies)

Analytical solution

Example: Analytical solution for intersection points of two quadrics

Problem

$$\mathbb{X} := \left\{ \mathbf{x} \in \mathbb{R}^2 \mid \underbrace{\mathbf{x}^\top \mathbf{A} \mathbf{x} + 2\mathbf{a}^\top \mathbf{x} + \alpha}_{=: Q_A(\mathbf{x})} = 0 \wedge \underbrace{\mathbf{x}^\top \mathbf{B} \mathbf{x} + 2\mathbf{b}^\top \mathbf{x} + \beta}_{=: Q_B(\mathbf{x})} = 0 \right\}$$

Solution: Relate both (e.g., if $\alpha \neq 0$ and $\beta \neq 0$)

$$Q_D(\mathbf{x}) := \frac{Q_A(\mathbf{x})}{\alpha} - \frac{Q_B(\mathbf{x})}{\beta} = \mathbf{x}^\top \underbrace{\left(\frac{\mathbf{A}}{\alpha} - \frac{\mathbf{B}}{\beta} \right)}_{=: \mathbf{D}} \mathbf{x} + 2 \underbrace{\left(\frac{\mathbf{a}}{\alpha} - \frac{\mathbf{b}}{\beta} \right)^\top}_{=: \mathbf{d}^\top} \mathbf{x} + \underbrace{\left(\frac{\alpha}{\alpha} - \frac{\beta}{\beta} \right)}_{=0} = 0$$

and note that

$$Q_D(\mathbf{x}) := \mathbf{x}^\top \left(\underbrace{\mathbf{D} \mathbf{x} + 2\mathbf{d}}_{\stackrel{!}{=} \lambda \mathbf{J} \mathbf{x}} \right) \stackrel{!}{=} 0 \iff \mathbf{x}^\star(\lambda) = -2(\mathbf{D} - \lambda \mathbf{J})^{-1} \mathbf{d}$$

Analytical solution

Example: Analytical solution for intersection points of two quadrics (cont'd)

then insert $\mathbf{x}^*(\lambda)$ in $Q_A(\mathbf{x})$ (or $Q_B(\mathbf{x})$), i.e.

$$Q_A(\mathbf{x}^*(\lambda)) = 4\mathbf{d}^\top (\mathbf{D} - \lambda \mathbf{J})^{-\top} \mathbf{A} (\mathbf{D} - \lambda \mathbf{J})^{-1} \mathbf{d} - 4\mathbf{a}^\top (\mathbf{D} - \lambda \mathbf{J})^{-1} \mathbf{d} + \alpha = 0 \quad \left| \cdot \underbrace{[\det(\mathbf{D} - \lambda \mathbf{J})]}_{\propto \lambda^2} \right|^2$$

$$\implies \boxed{\chi(\lambda) := c_4 \lambda^4 + c_3 \lambda^3 + c_2 \lambda^2 + c_1 \lambda + c_0 \stackrel{!}{=} 0}$$

$\implies$ Analytical (real) solutions $\lambda^* \in \{\lambda_1, \dots, \lambda_4\}$ can be computed [103]:

$$\implies \boxed{\mathbf{x}^*(\lambda^*) = -2(\mathbf{D} - \lambda^* \mathbf{J})^{-1} \mathbf{d}}$$

Implementation results

Laboratory setup

Reluctance SM (RSM) and Permanent-magnet SM



Host PC (rapid prototyping)

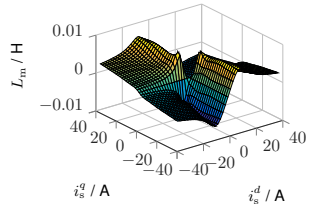
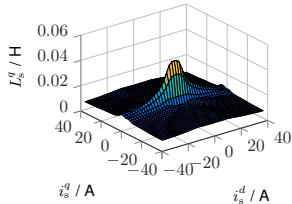
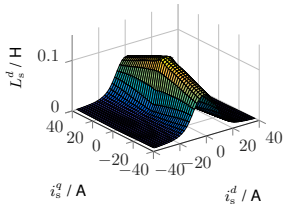
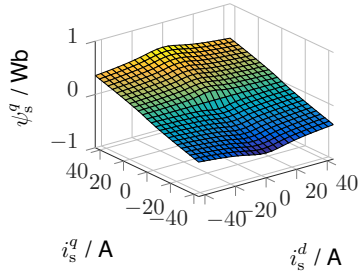
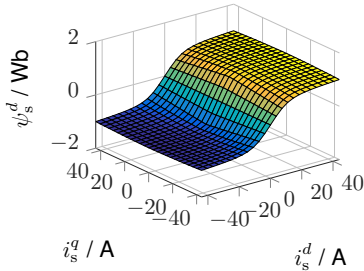


Real-time system and VSIs



Implementation results

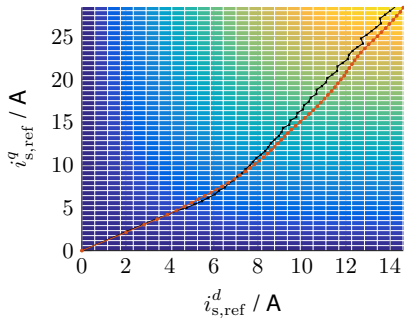
Nonlinear flux linkages and inductances of RSM



Implementation results

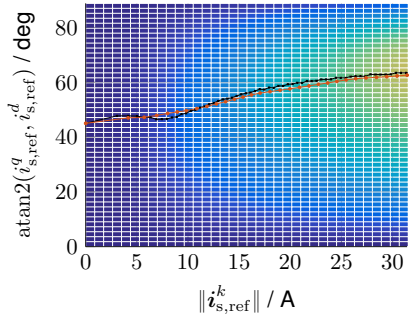
Comparison of numerical and analytical solutions for MTPC

m_m — numerical — analytical



Cartesian coordinates

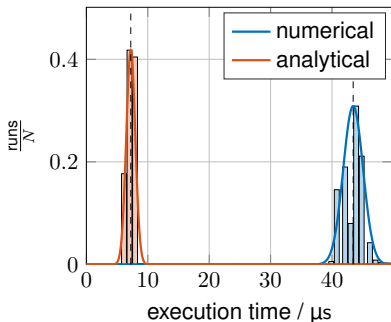
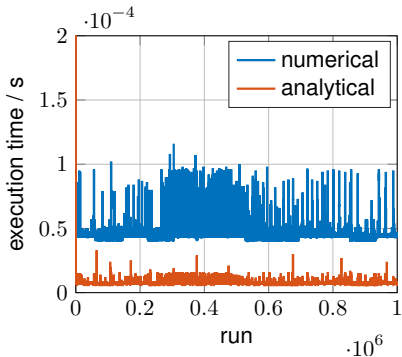
m_m — numerical — analytical



polar coordinates

Implementation results

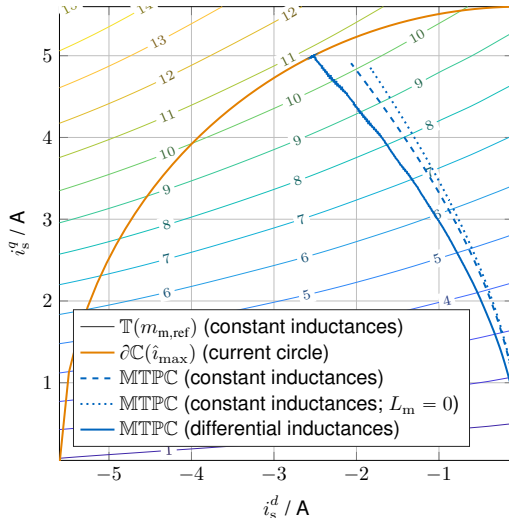
Comparison of the computational load (Euler's solution for fourth-order polynomials)



- Execution times for $N = 10^6$ runs (downsampled by factor 100);
- Average execution times $\mu_n = 43,4 \cdot 10^{-6}$ s and $\mu_a = 7,23 \cdot 10^{-6}$ s; and
- Standard deviations $\sigma_n = 1,61 \cdot 10^{-6}$ s and $\sigma_a = 0,73 \cdot 10^{-6}$ s.

Implementation results

MTPC at a IPMSM with non-negligible mutual inductance and nonlinear flux linkage



Conclusion

Summary and future work

To take home

- **unified** theory for MTPC, FW, MTPV/MTPF or MC based on
 - **quadrics** (implicit formulation),
 - **optimization problems** with **equality constraint**, and
 - **intersection** of two quadrics
- **analytical** solution for reference currents (& transition points)
- $R_s \neq 0$ and $L_m \neq 0$ (both can be considered **simultaneously**)
- **fast(er)** and **more accurate** computation
- **applicable** in real-world (nonlinear RSM and IPMSM)

Future work

- convergence (mathematical proof or consideration of nonlinear flux linkages)
- consideration of iron losses (including e.g. $R_{fe}(\omega_k)$; article in preparation)
- impact of parameter uncertainty (e.g. $R_s^a \neq R_s^b \neq R_s^c$; article in preparation)

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