

Funnel control with disturbance observer for two-mass systems

Christoph Hackl

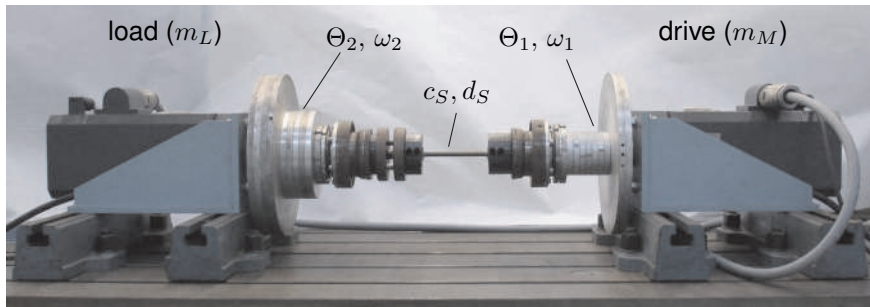
Technische Universität München
Institute for Electrical Drive Systems and Power Electronics

52nd IEEE Conference on Decision and Control, Florence
13th December 2013

Outline

- 1 Problem statement
- 2 Funnel control (FC) for two-mass systems (2MS)
- 3 FC with disturbance observer for two-mass systems
- 4 Conclusions and future work

Problem: Speed control of a two-mass system (2MS)

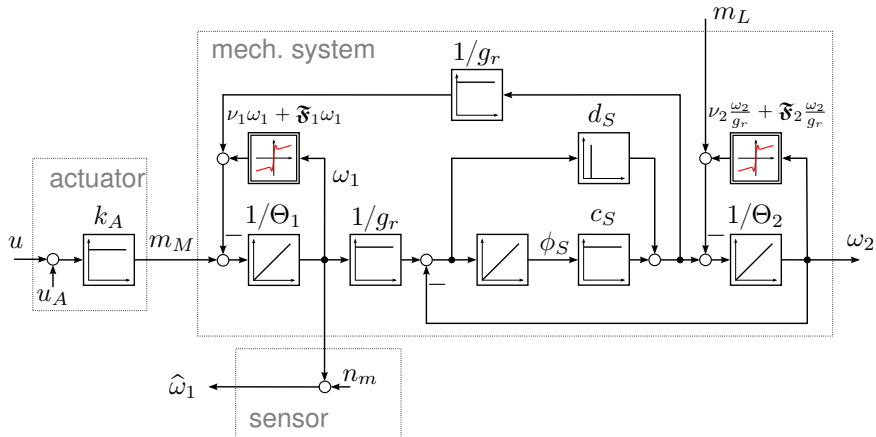


- reference tracking $\omega_2 \rightarrow \omega_{2,\text{ref}}$ (or $\omega_1 \rightarrow \omega_{1,\text{ref}}$)
- active damping of natural frequency

$$\omega_0 = \sqrt{\frac{c_S(\Theta_1 + \Theta_2)}{\Theta_1\Theta_2}} \approx 61 \text{ [rad/s]} \quad \implies \quad f_0 \approx 9.7 \text{ [Hz]}$$

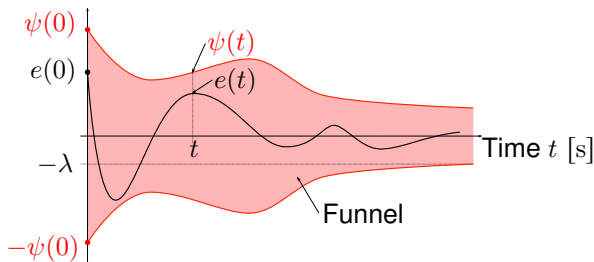
- ω_1 as feedback signal only

Two-mass system model



$$\left. \begin{aligned} \frac{d}{dt} \mathbf{x}_S(t) &= \mathbf{A}_S \mathbf{x}_S(t) + \mathbf{b}_S (u(t) + u_A(t)) + \mathbf{B}_S \begin{pmatrix} (\mathfrak{F}_1 \omega_1)(t) \\ m_L(t) + (\mathfrak{F}_2 \omega_2)(t) \end{pmatrix}, \\ y(t) &= (1, 0, 0) \mathbf{x}_S(t), \quad \mathbf{x}_S(0) = (\omega_1^0, \phi_S^0, \omega_2^0) \in \mathbb{R}^3 \end{aligned} \right\} \quad (2MS)$$

Funnel control [Ilchmann et al., 2002]



- Tracking with prescribed transient accuracy by design of $\psi(\cdot)$, i.e.

$$\forall t \geq 0: \quad |e(t)| = |y_{\text{ref}}(t) - y(t)| < \psi(t)$$

- Controller

$$u(t) = \underbrace{\frac{1}{\psi(t) - |e(t)|}}_{=:k(t)} e(t)$$

Admissible system class $\mathcal{S}$ (simplified)

System

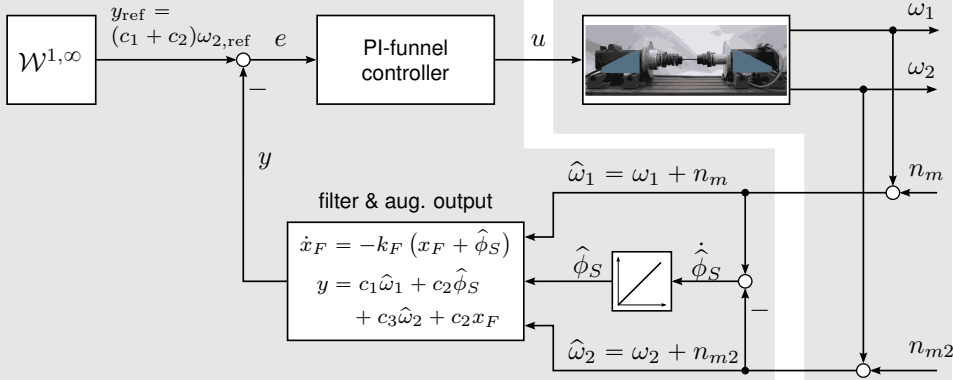
$$\left. \begin{aligned} \dot{\mathbf{x}}(t) &= \mathbf{A}\mathbf{x}(t) + \mathbf{b}(u(t) + u_d(t)) + \mathbf{B}\mathfrak{T}\left(\mathbf{d}(t) + (\mathfrak{T}\mathbf{x})(t)\right) \\ y(t) &= \mathbf{c}^\top \mathbf{x}(t), \end{aligned} \right\} \quad (1)$$

satisfying

- (i) $\gamma_0 := \mathbf{c}^\top \mathbf{b} \neq 0$ and $\text{sign}(\gamma_0)$ known;
- (ii) $\forall s \in \mathbb{C}$ with $\Re(s) \geq 0$: $\det \begin{bmatrix} s\mathbf{I}_n - \mathbf{A} & \mathbf{b} \\ \mathbf{c}^\top & 0 \end{bmatrix} \neq 0$;
- (iii) operator $\mathfrak{T}$ is of class $\mathcal{T}$ (see Def. 1 in Ilchmann et al. [2002]) and $M_{\mathfrak{T}} := \sup \{ \|(\mathfrak{T}\xi)(t)\| \mid t \geq 0, \xi(\cdot) \in \mathcal{C}([-h, \infty), \mathbb{R}^n) \} < \infty$;
- (iv) $u_d(\cdot) \in \mathcal{L}^\infty([-h, \infty); \mathbb{R})$ and $\mathbf{d}(\cdot) \in \mathcal{L}^\infty([-h, \infty); \mathbb{R}^m)$.

Funnel control for 2MS [Ilchmann and Schuster, 2009]

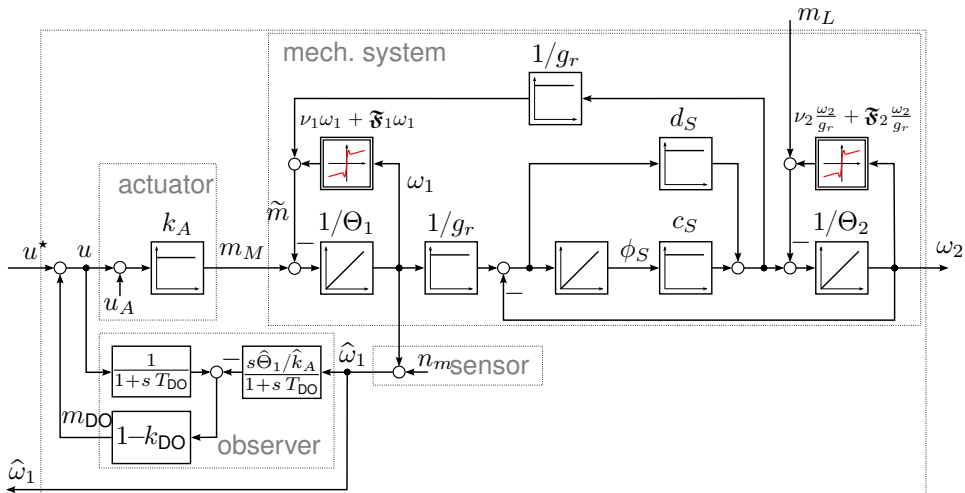
implementation in xPC target



$$\boxed{2\text{MS} \in \mathcal{S}} \iff c_1 > 0 \wedge \frac{c_2}{g_r} \geq 0 \wedge \frac{c_3}{g_r} > -c_1 \wedge k_F > 0.$$

For active damping: Feedback of ω_1 and ω_2 necessary!

2MS with disturbance observer (DO) [Hori et al., 1999]



$$m_{DO}(s) = \frac{\tilde{m}(s)}{k_A} - u_A(s) \quad (\text{for } \hat{k}_A = k_A, \hat{\Theta}_1 = \Theta_1, k_{DO} = T_{DO} = n_m = 0)$$

2MS with disturbance observer element of class $\mathcal{S}$

Extended two-mass system with $\mathbf{x} = (\omega_1, \phi_S, \omega_2, x_F)^\top$

$$\left. \begin{aligned} \frac{d}{dt} \mathbf{x}(t) &= \mathbf{A}\mathbf{x}(t) + \mathbf{b}(u^*(t) + u_A(t)) + \mathbf{B} \begin{pmatrix} (\mathfrak{F}_1 \omega_1)(t) \\ m_L(t) + (\mathfrak{F}_2 \omega_2)(t) \end{pmatrix}, \\ y(t) &= \mathbf{c}^\top \mathbf{x}(t), \quad \mathbf{x}(0) = ((\mathbf{x}_S^0)^\top, 0)^\top \in \mathbb{R}^4 \end{aligned} \right\} \quad (2)$$

where $\mathbf{A} = \begin{bmatrix} \mathbf{A}_S & \star \\ \star & -\frac{k_{DO}}{T_{DO}} \end{bmatrix}$, $\mathbf{b} = \begin{pmatrix} \mathbf{b}_S \\ \frac{1}{T_{DO}} \end{pmatrix}$, $\mathbf{B} = \begin{bmatrix} \mathbf{B}_S \\ 0, 0 \end{bmatrix}$ and $\mathbf{c}^\top = (1, 0, 0, 0)$.

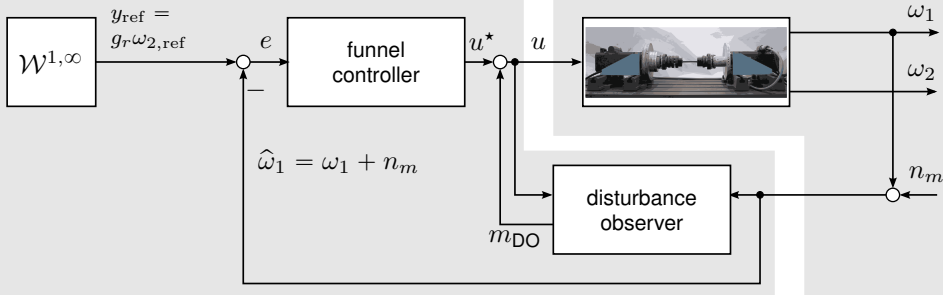
Proposition

For $T_{DO} > 0$, $k_{DO} \in \mathbb{R}$, $\hat{k}_A > 0$ and $\hat{\Theta}_1 > 0$, the extended two-mass system (2) is element of system class $\mathcal{S}$.

Proof by checking system properties (i)–(iv) of system class $\mathcal{S}$.

Implementation

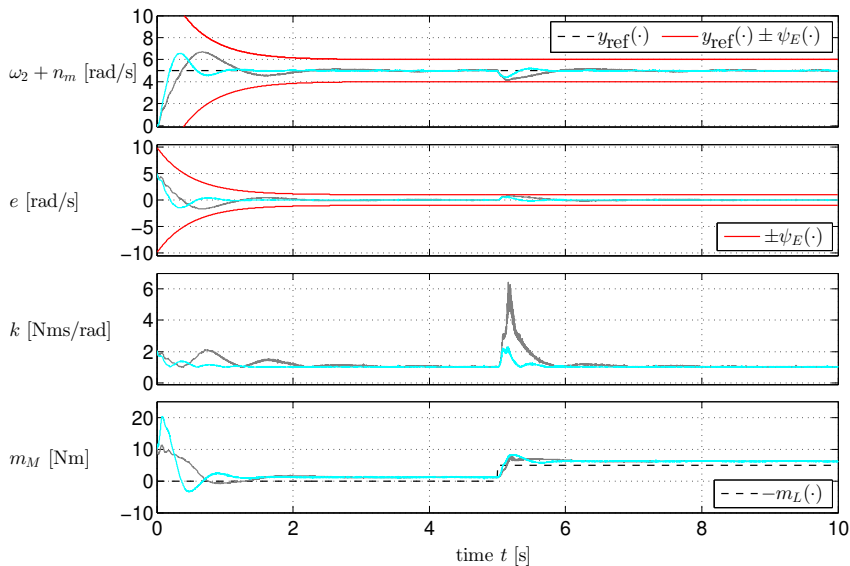
implementation in xPC target



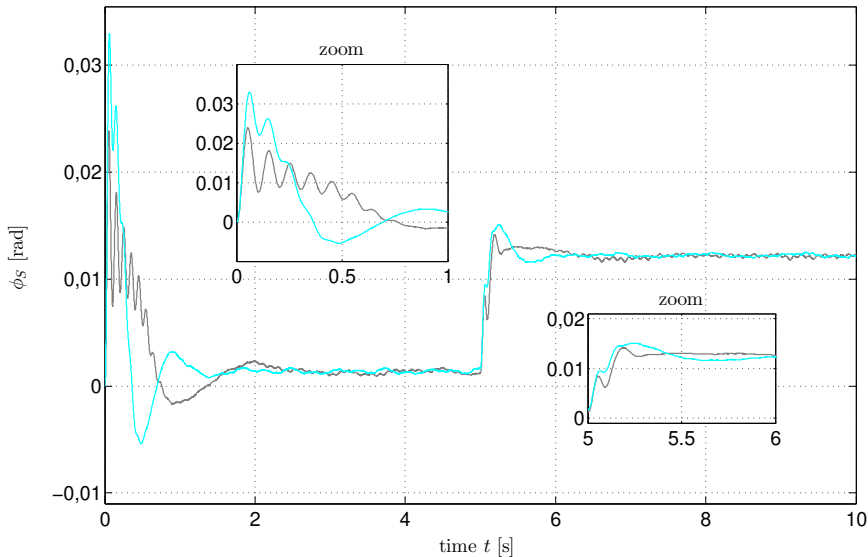
Disturbance observer design

$$k_{\text{DO}} = 0 \quad \wedge \quad T_{\text{DO}} = 0.03 \text{ [s]} \quad \left(\frac{1}{T_{\text{DO}}} = 33.3 \text{ [Hz]} > f_0 = 9.7 \text{ [Hz]} \right)$$

Measurement results: — PI+FC, — FC+DO



Meas. results (zoom): — PI+FC, — FC+DO



Conclusions and future work

To take home:

- Funnel control with disturbance observer admissible for 2MS (mathematical and experimental validation)
- Active damping of oscillations
- Tracking with prescribed transient accuracy (on motor side)

Open questions:

- ... impact of actuator saturation?
- ... prescribed accuracy also for load side?
- ... other (disturbance) observer designs admissible and beneficial?

References

- Y. Hori, H. Sawada, and Y. Chun. Slow resonance ratio control for vibration suppression and disturbance rejection in torsional system. *IEEE Transactions on Industrial Electronics*, 46(1): 162–168, 1999.
- A. Ilchmann and H. Schuster. PI-funnel control for two mass systems. *IEEE Transactions on Automatic Control*, 54(4):918–923, 2009.
- A. Ilchmann, E. P. Ryan, and C. J. Sangwin. Tracking with prescribed transient behaviour. *ESAIM: Control, Optimisation and Calculus of Variations*, 7:471–493, 2002.